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**NAFEMS - FENET Workshop  
13-14 June 2002, Zurich**

**Fatigue Life Improvement of  
an Innovative Suspension System**

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**Technical Manager**

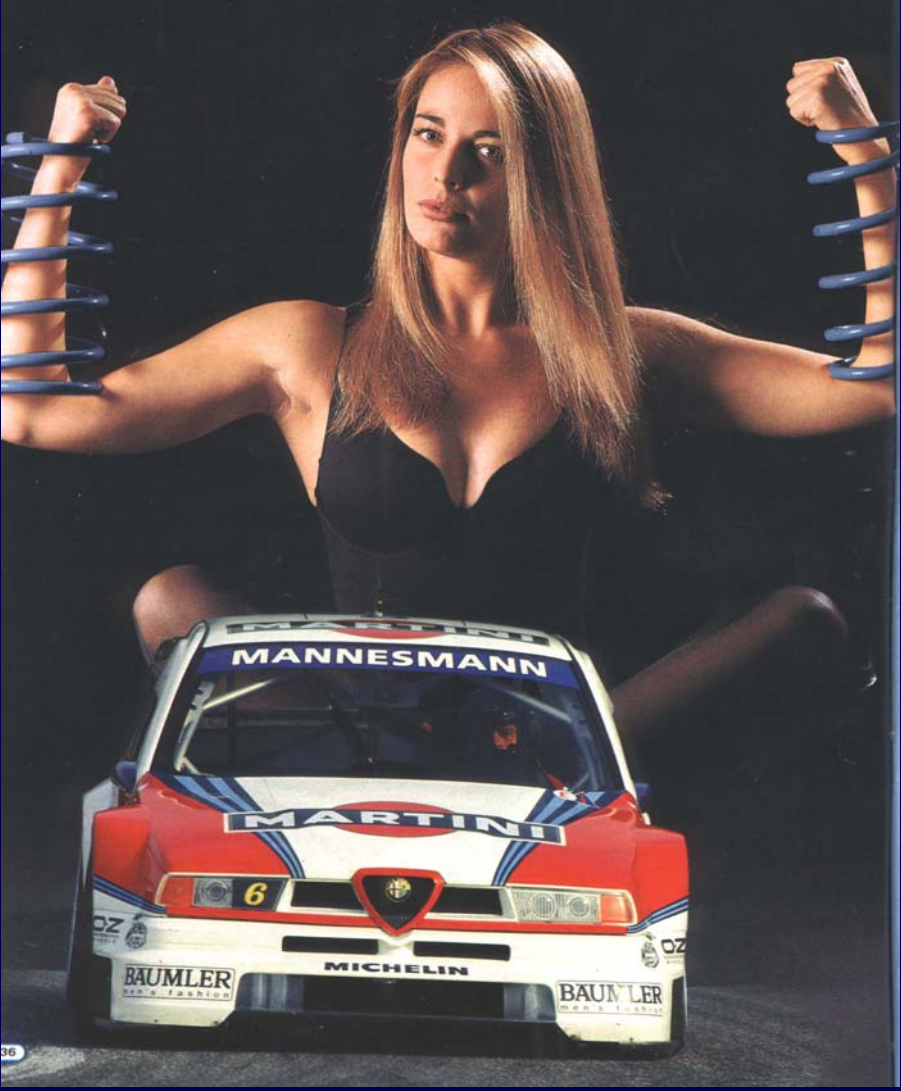
**NNC Limited**

**UK**

# Models for the Automotive Industry



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# Contents



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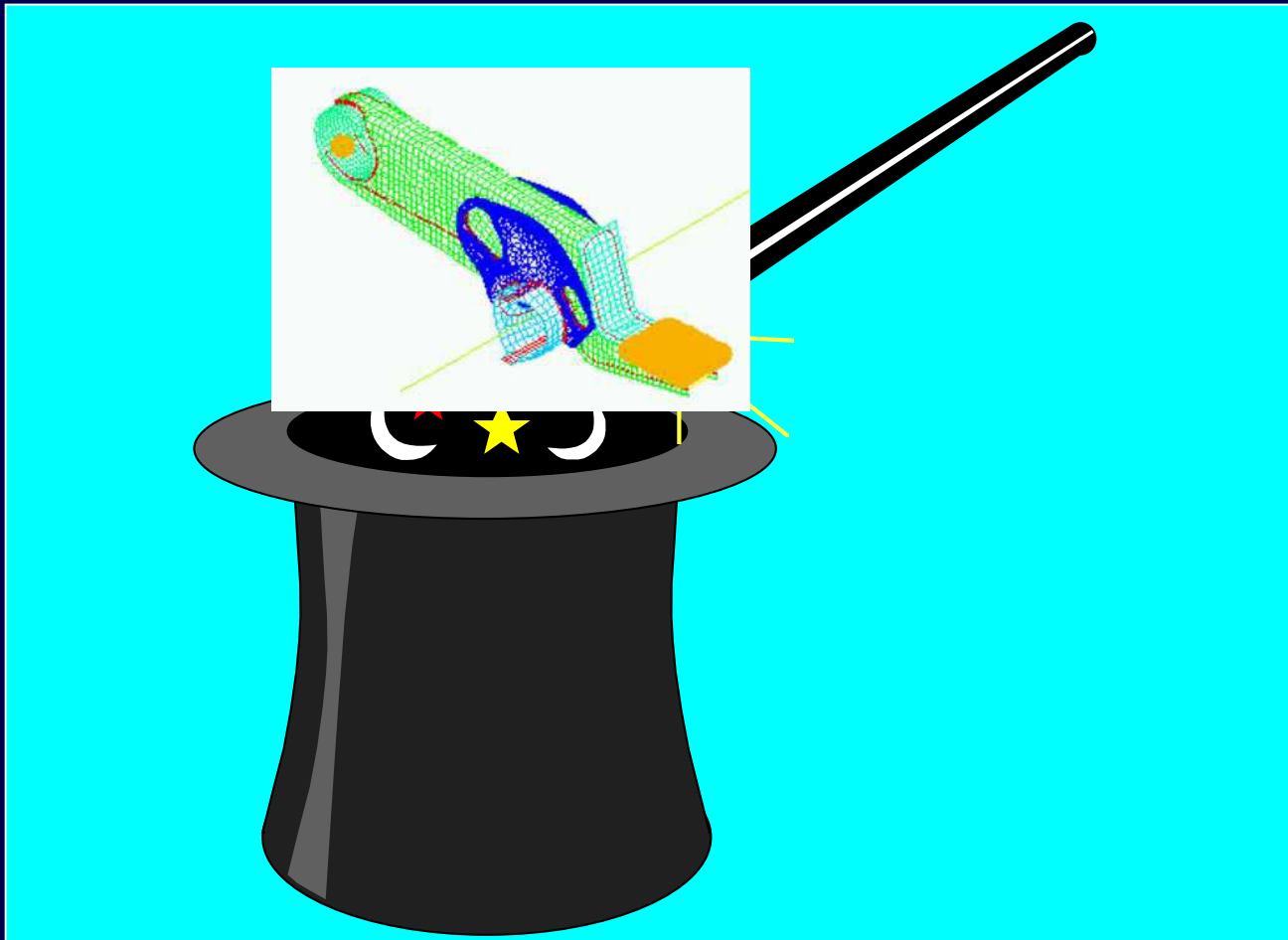
- **Introduction**
- **Methodology**
- **Model Geometry**
- **Stress Analysis**
- **Fatigue Assessment**
- **Recommendations**
- **Conclusions**

"We are testing are 5th prototype. What magic can you do?"



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## FE Modelling



## History

New designs for suspension systems for lorries were being developed by conventional test and trial method

## Scope of Work

To use Finite Element analysis to improve the fatigue life of the Suspension Assembly.

## Objectives

- Failure assessment of Mark V Suspension System.
- Demonstrate capabilities of complex FE analysis techniques to support design development.
- Suggest design improvements.
- Streamline design development process.

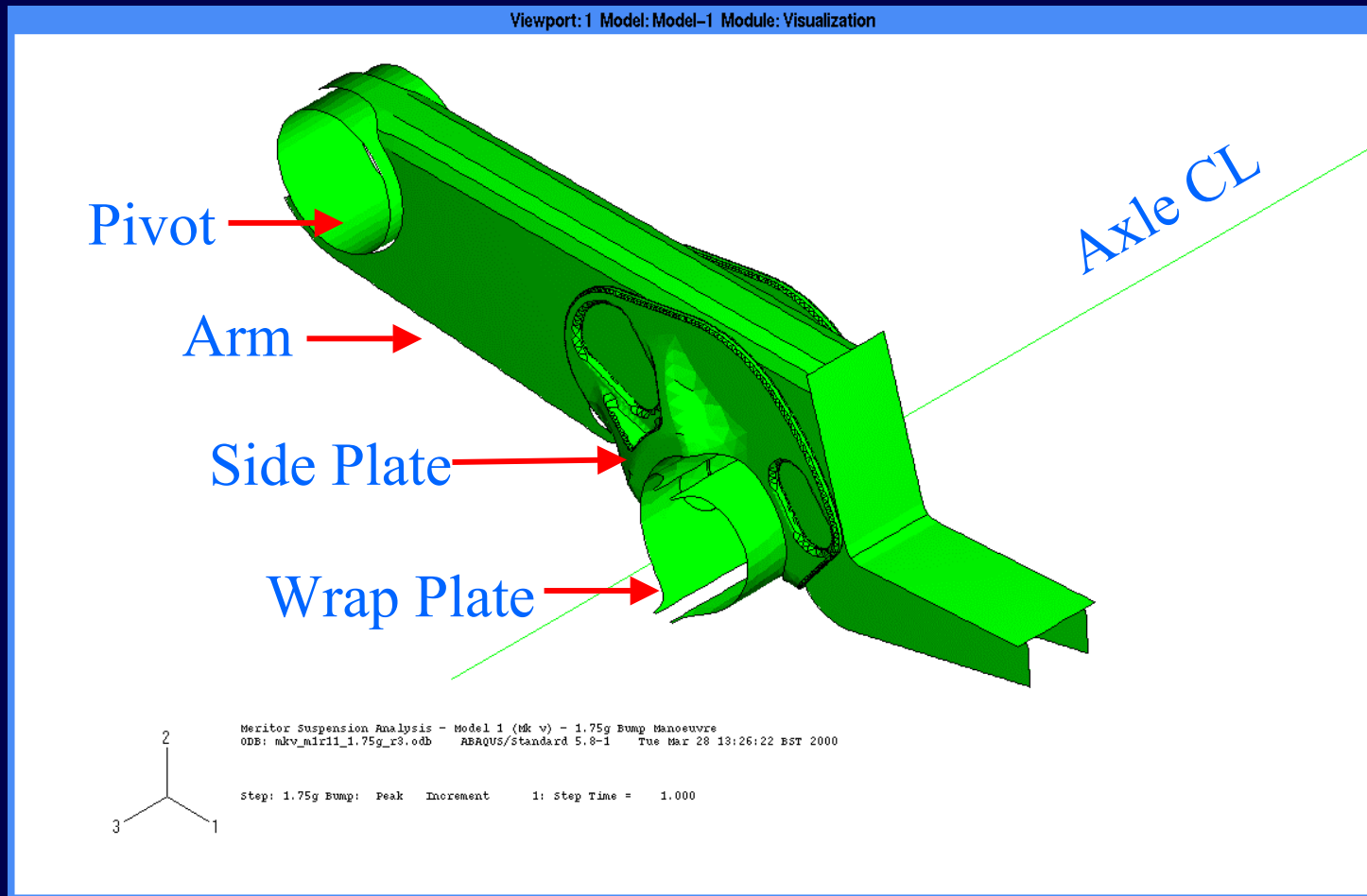
- **Convert CAD geometry to FE model**
  - mid-surfaces/volumes
  - meshing
  - boundary conditions/loading
  - validation
- **Stress Analysis**
- **Fatigue Analysis**
- **Assessment**
  - Steel components
  - Welded joints

# Main Components



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## Assembled in parts for easier manufacturing

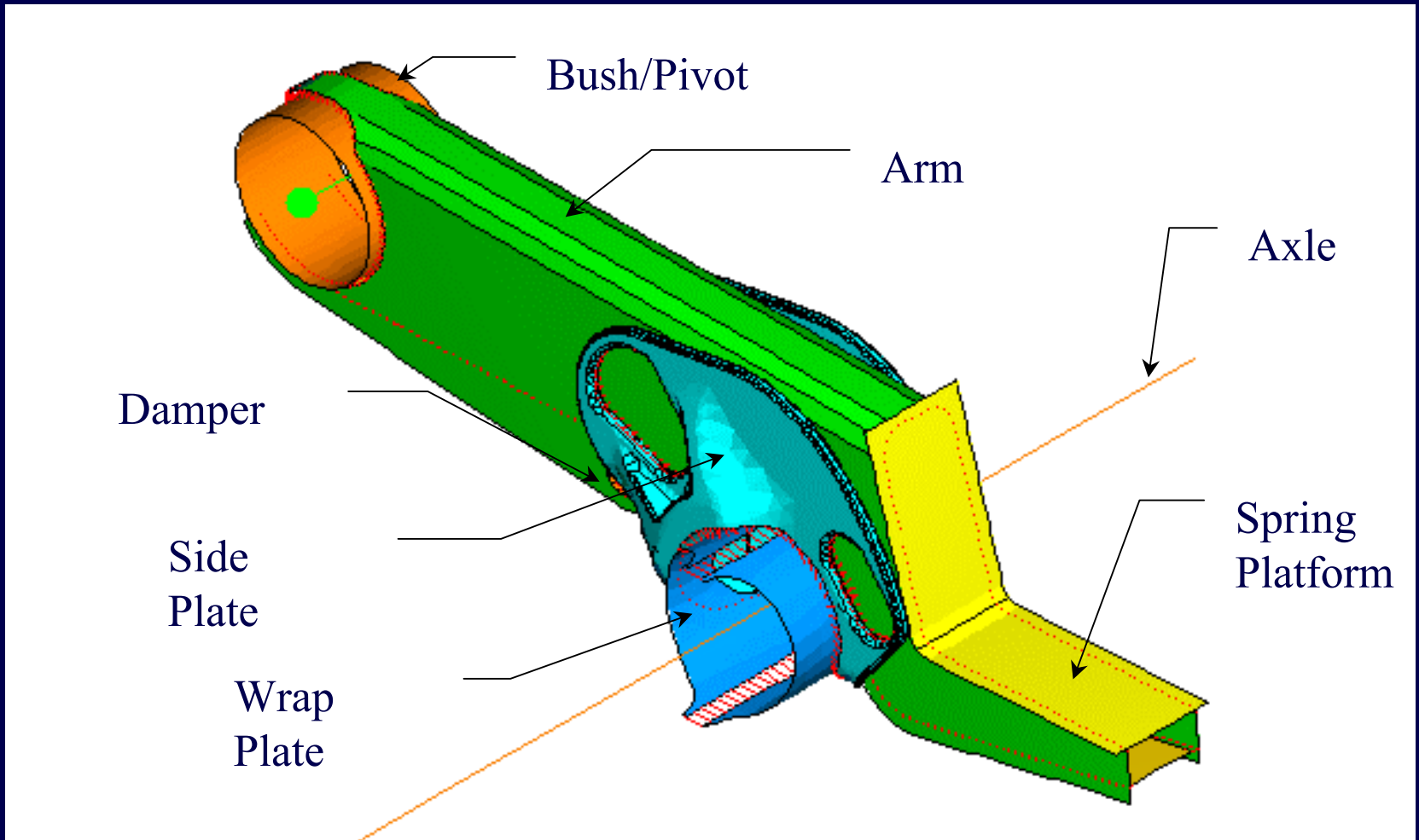




# Model Geometry - Parts



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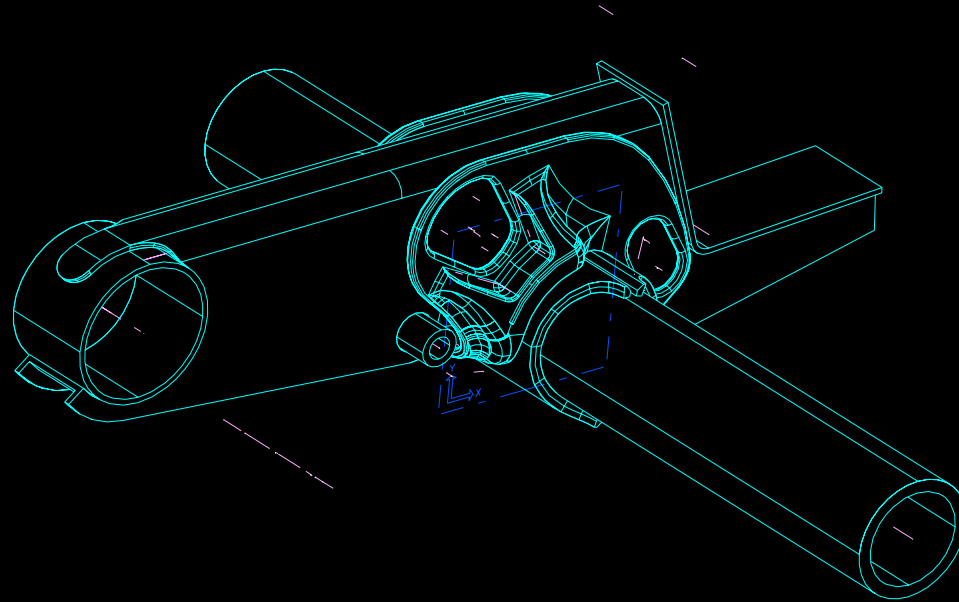


# Model Geometry - From CAD to FE



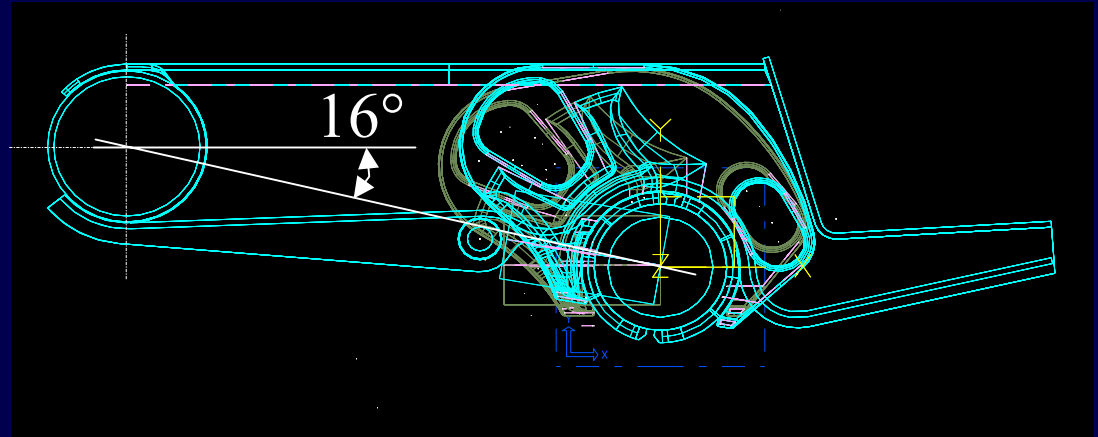
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## IGES File - Volumes

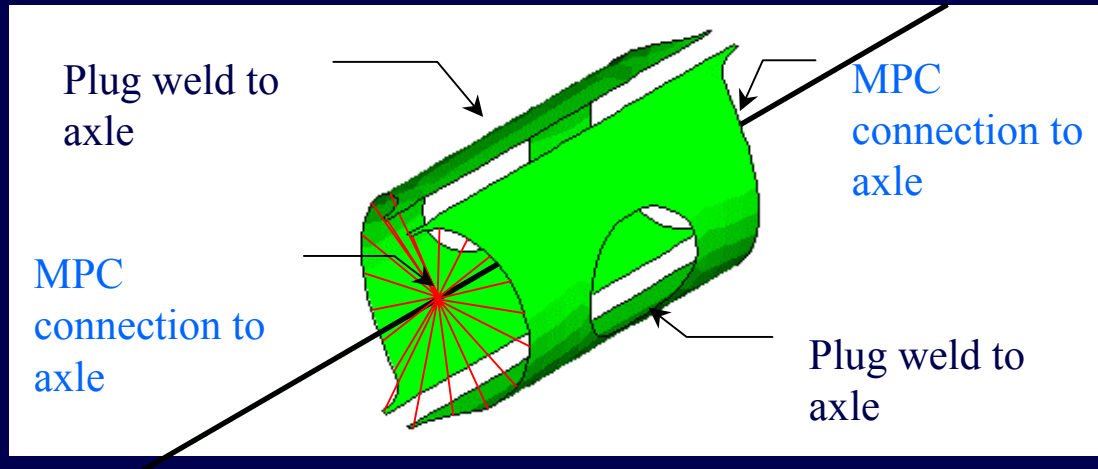


# Modelling Assumptions

- Orientation of Side Plate
- Angle @ start of test 20°



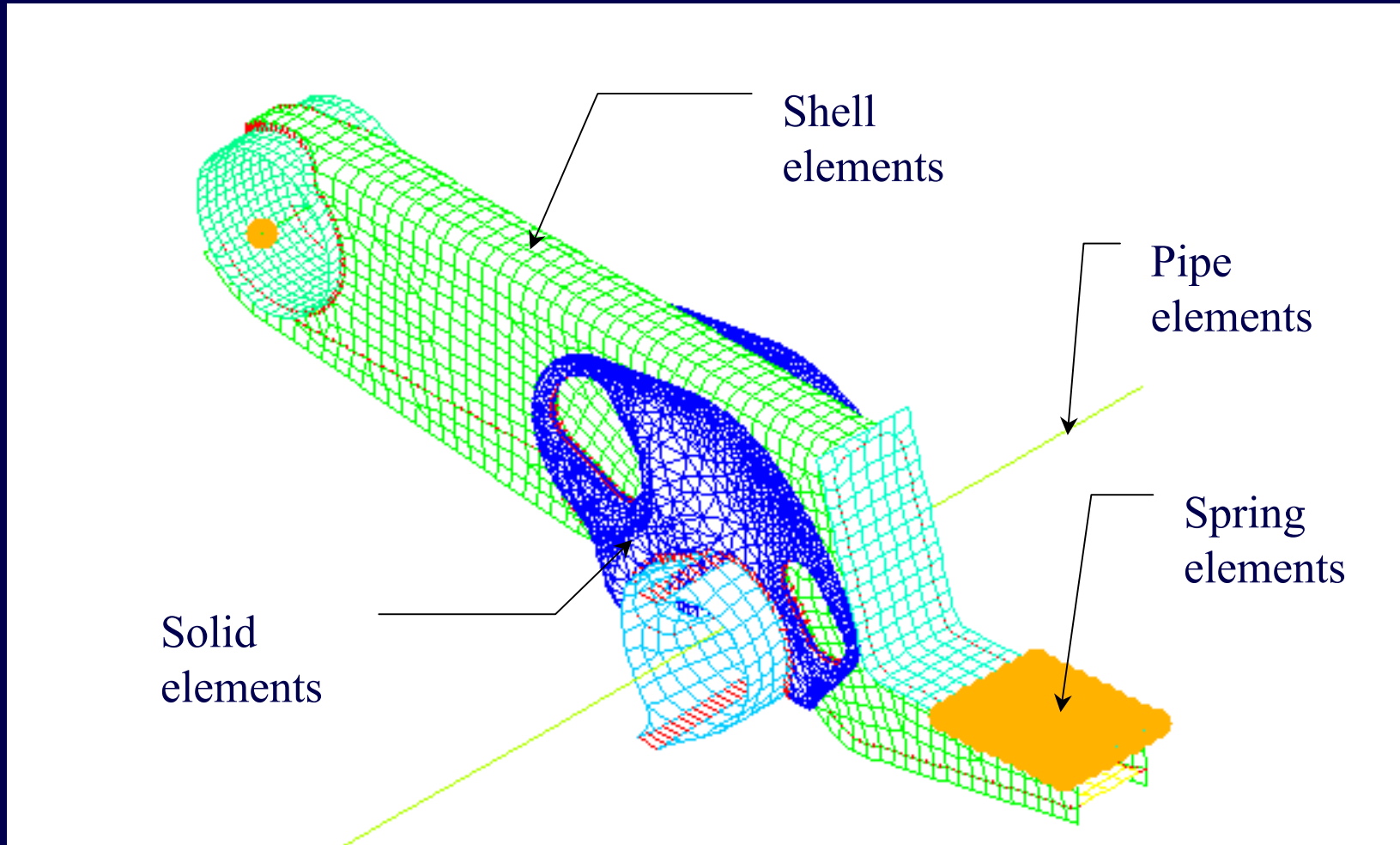
- Axle to Wrap Plate connection- No frictional contact



# Model Geometry - Mesh Generation

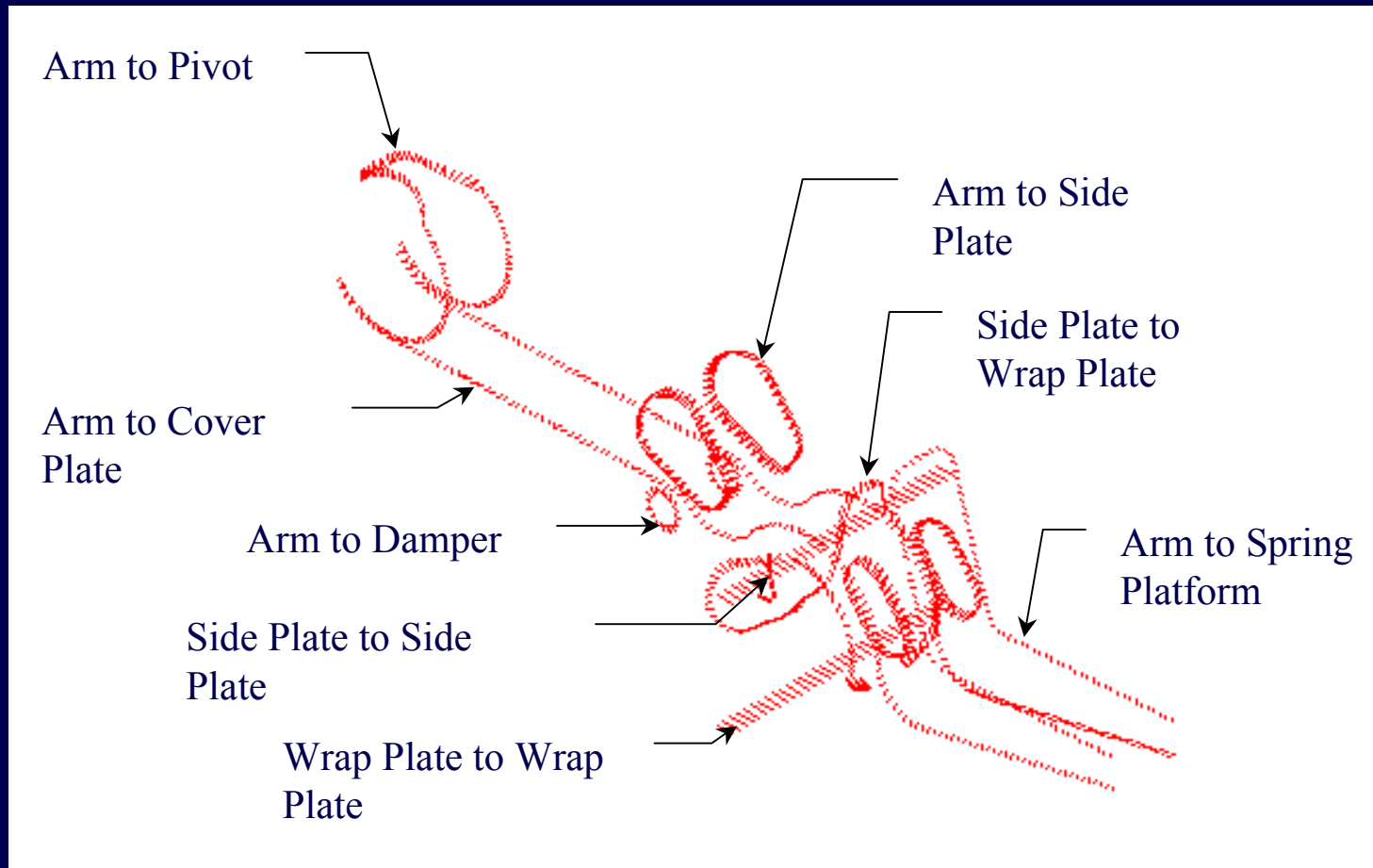


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# Modelling of Welded Joints

- Welds represented as Beam Elements

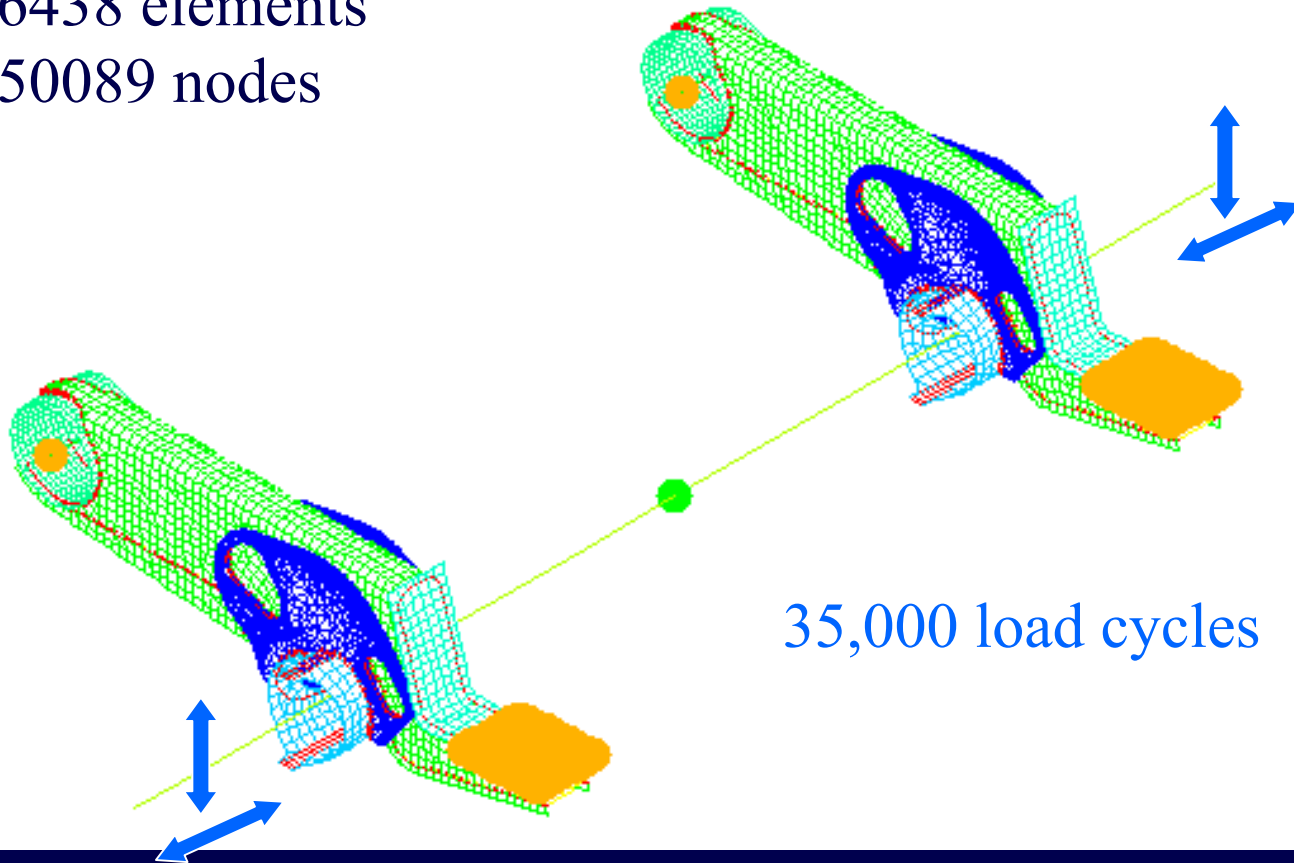


# Mesh Generation - Full Model



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86438 elements  
150089 nodes



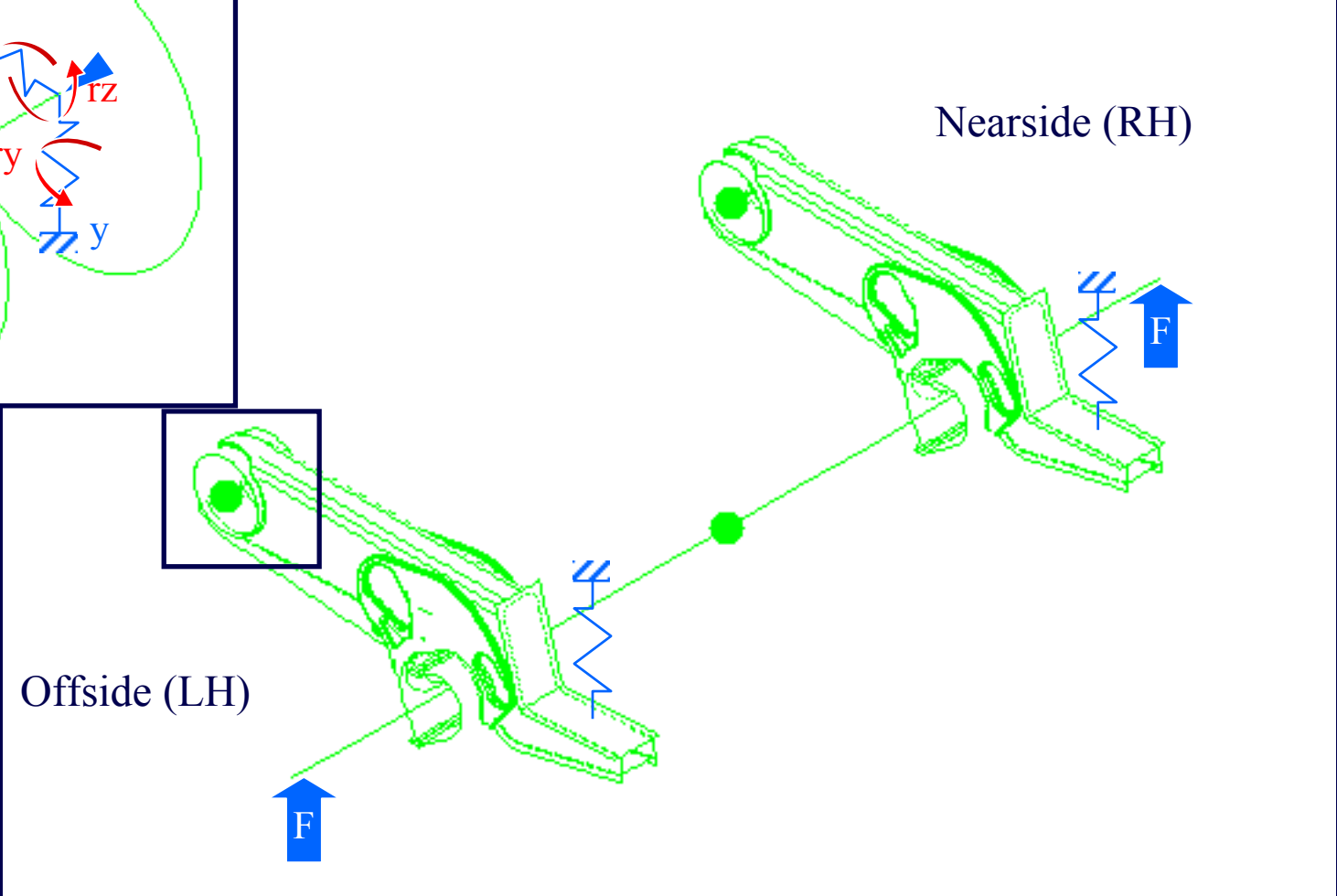
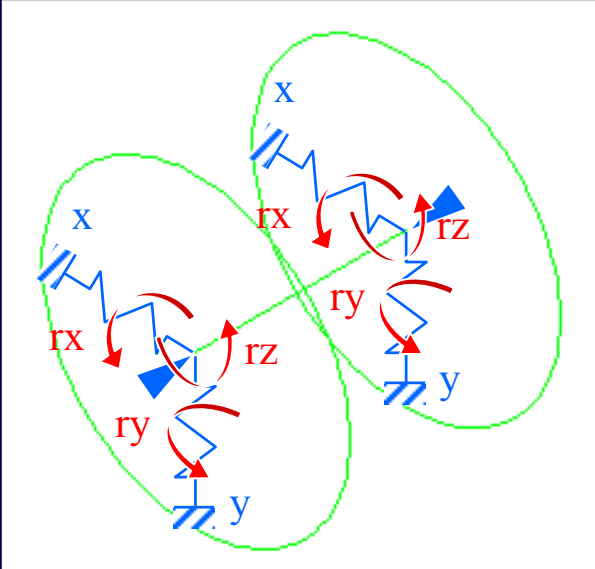
35,000 load cycles

- **Linear Elastic**
  
- **Boundary Conditions**
  
- **4 Loadcases**
  - **Roll Manoeuvre**
  - **Tramp Manoeuvre**
  - **Scrub Manoeuvre**
  - **1.75g Bump Manoeuvre**
  
- **Material Properties**

# Stress Analysis - Boundary Conditions



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# Stress Analysis - Material Properties



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| Part            | Young's Modulus | Poisson's Ratio |
|-----------------|-----------------|-----------------|
| Arm             | 203GPa          | 0.3             |
| Spring Platform | "               | "               |
| Cover Plate     | "               | "               |
| Damper          | "               | "               |
| Side Plate      | "               | "               |
| Wrap Plate      | "               | "               |
| Pivot           | "               | "               |
| Welds           | 406GPa          | "               |
| Axle            | 203GPa          | "               |

# Stress Analysis - Loadcase 1



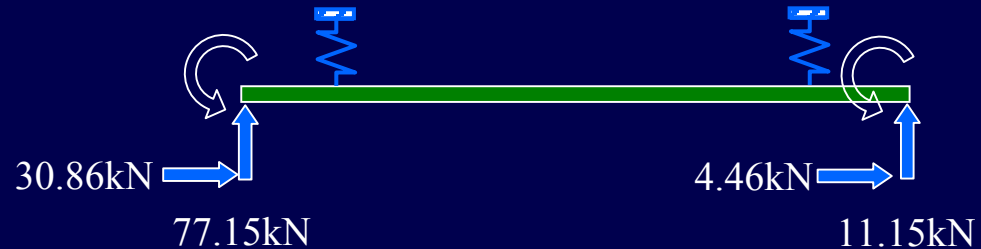
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## ■ Roll Manoeuvre

- Start **Step 1**
- Mid
- End



- Rollover **Step 2**



- Rollover **Step 3**



# Stress Analysis - Loadcase 2



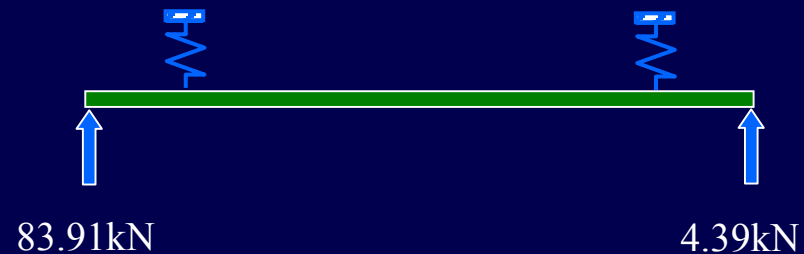
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## ■ Tramp Manoeuvre

- Start **Step 1**
- Mid
- End



- LH Bump **Step 2**



- RH Bump **Step 3**



# Stress Analysis - Loadcase 3



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## ■ Scrub Manoeuvre

- Start **Step 1**
- Mid
- End



- LH +ve **Step 2**



- LH -ve **Step 3**



# Stress Analysis - Loadcase 4



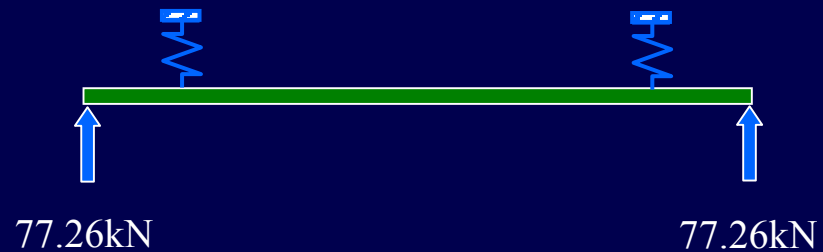
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## ■ 1.75g Bump Manoeuvre

- Start **Step 1**
- End



- Peak **Step 2**



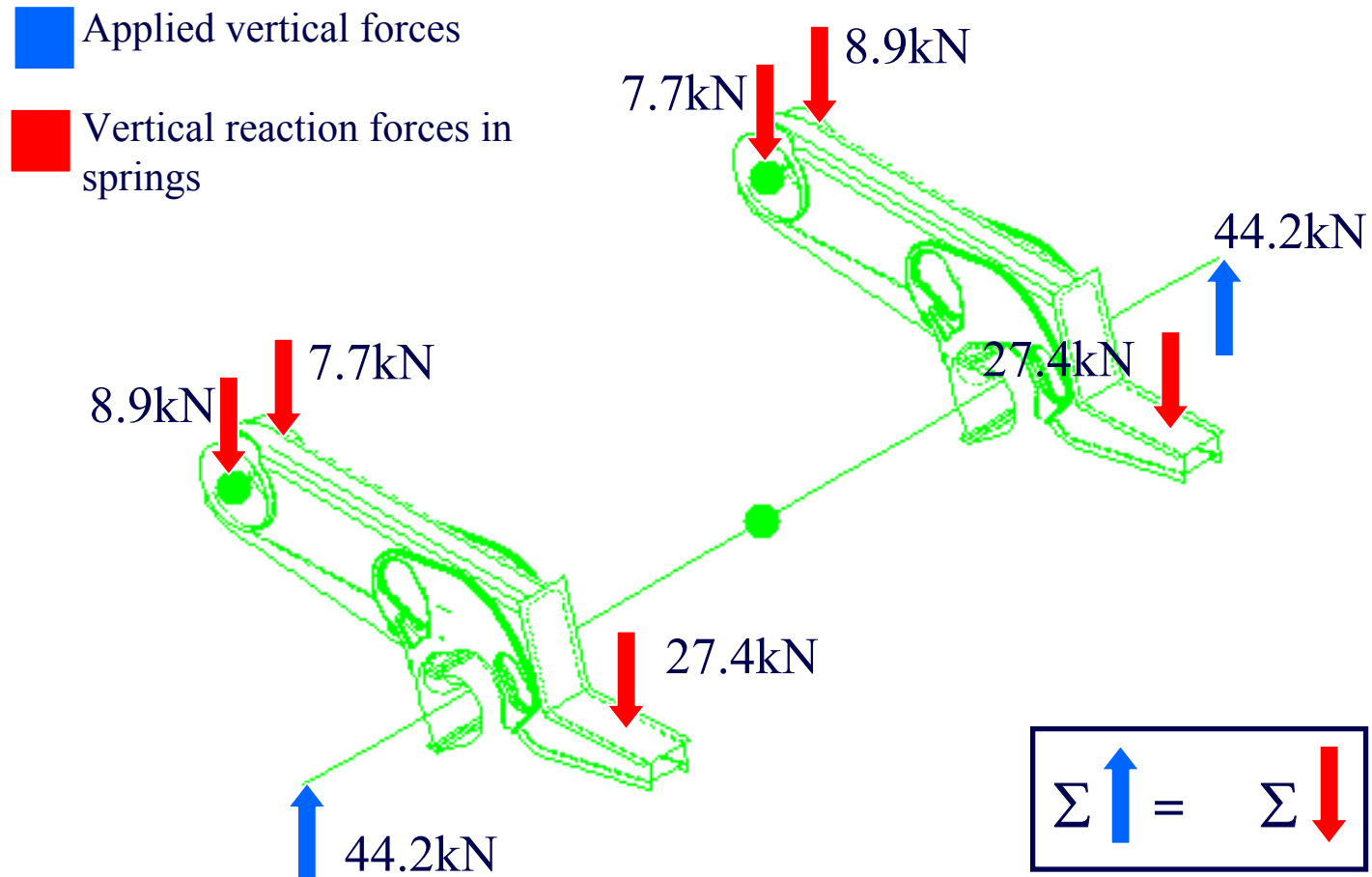


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# **Loadcase 1: Roll Manoeuvre**

# Stress Analysis - Model Validation

## Start Condition - Sum of Vertical Forces

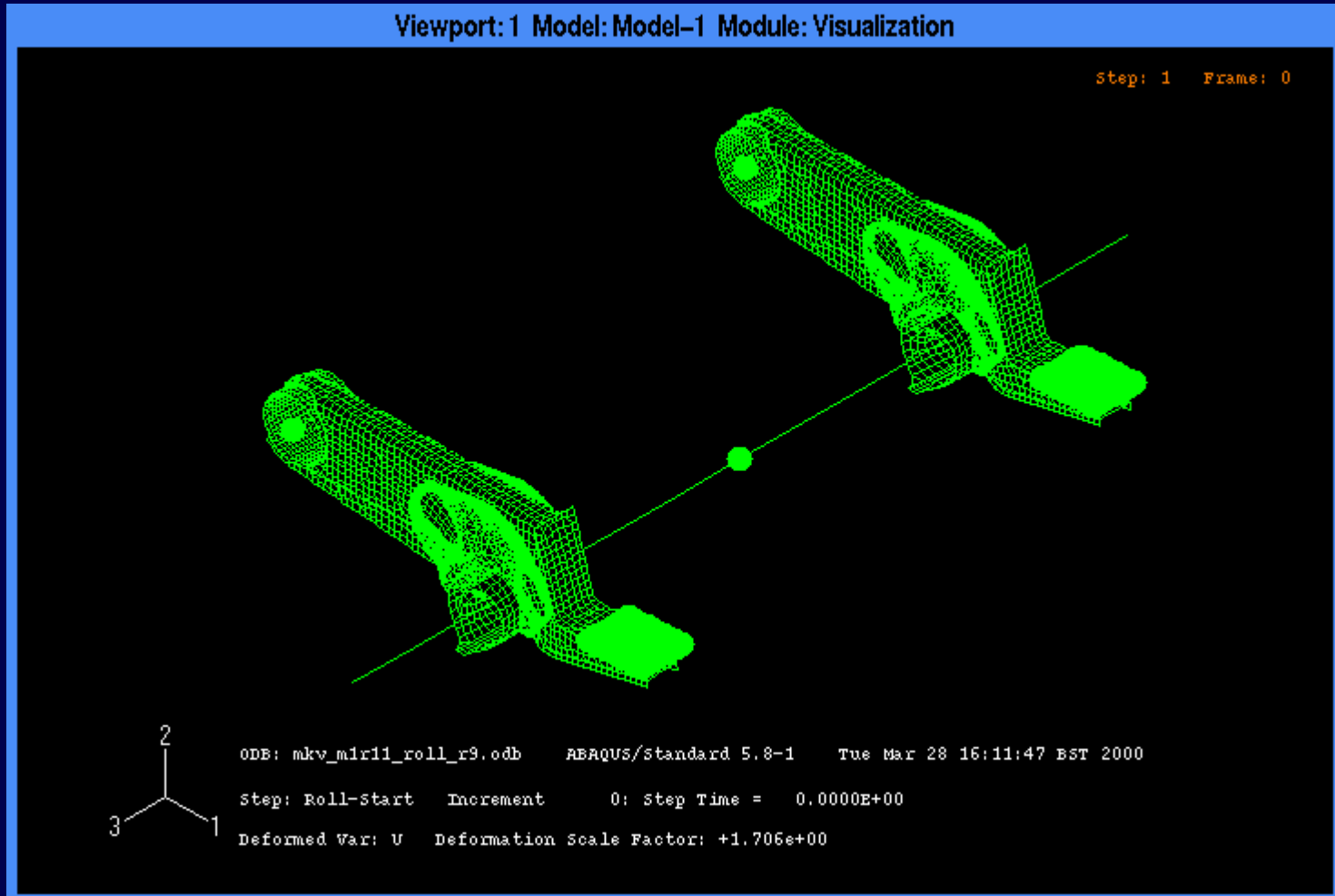


# Stress Analysis - Results



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## ■ Roll Manoeuvre - Displaced Shape



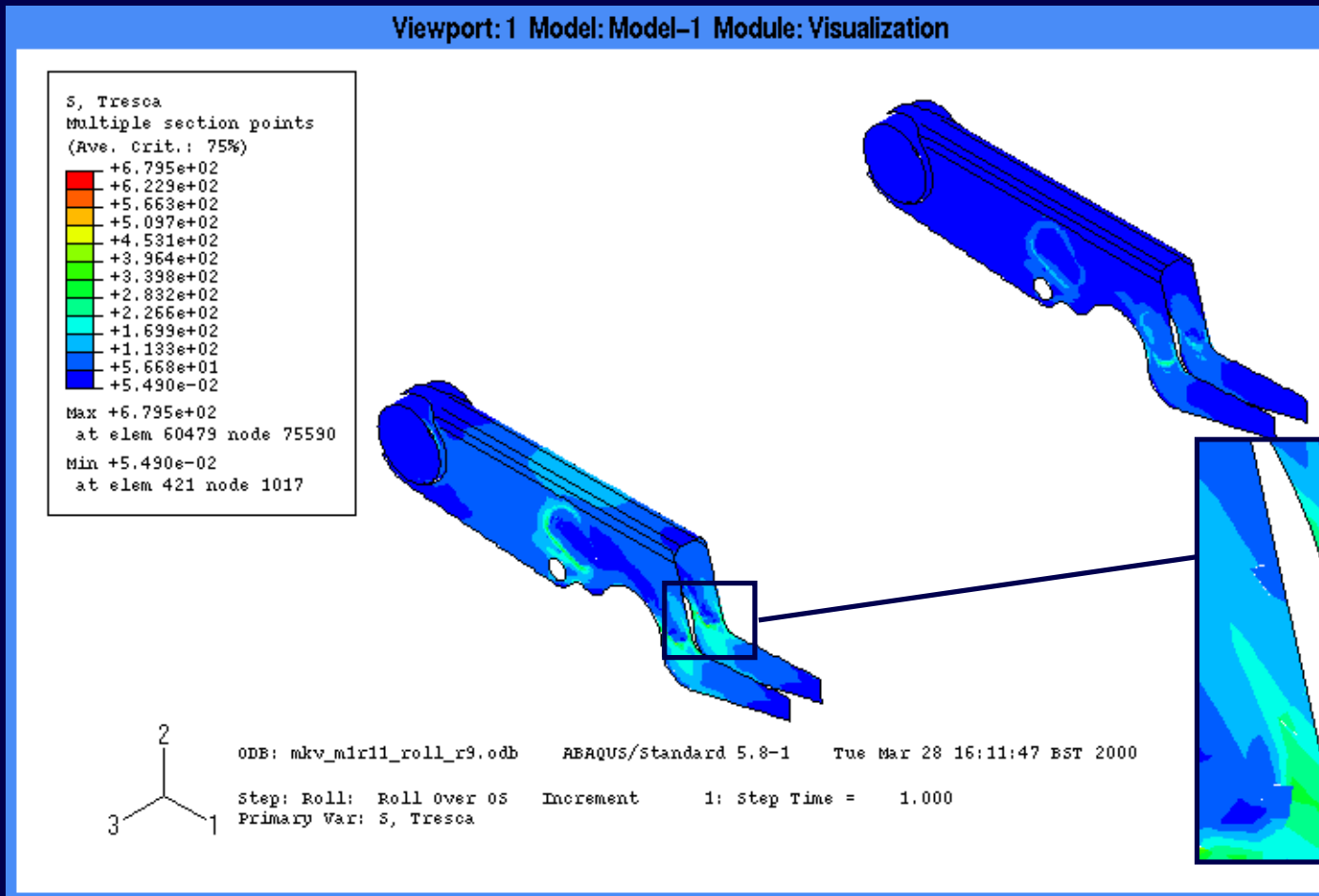


# Stress Analysis - Results



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## ■ Rollover LH - Arm/Pivot - TRESCA Stress

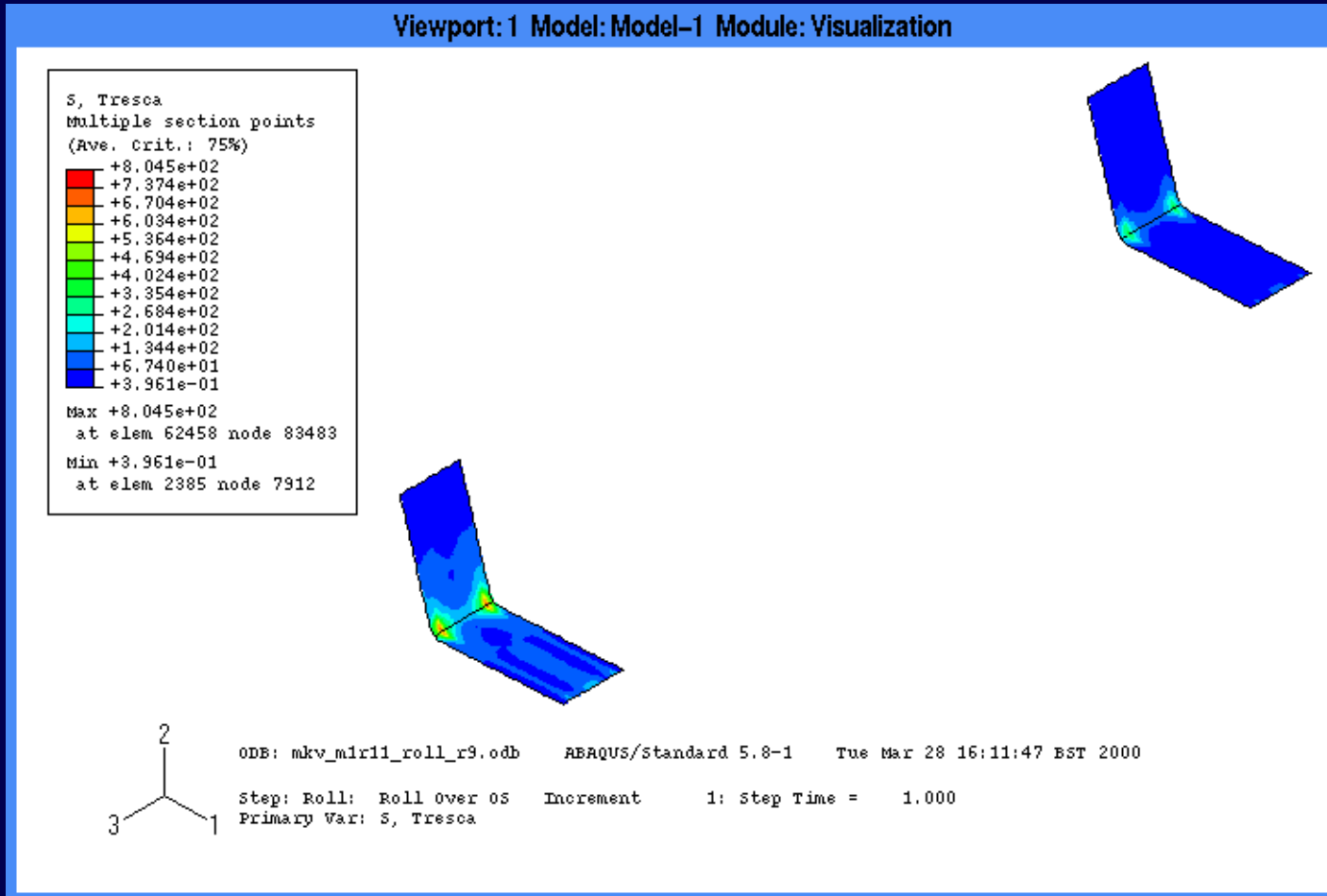


# Stress Analysis - Results



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## ■ Rollover LH - Spring Platform - TRESCA Stress

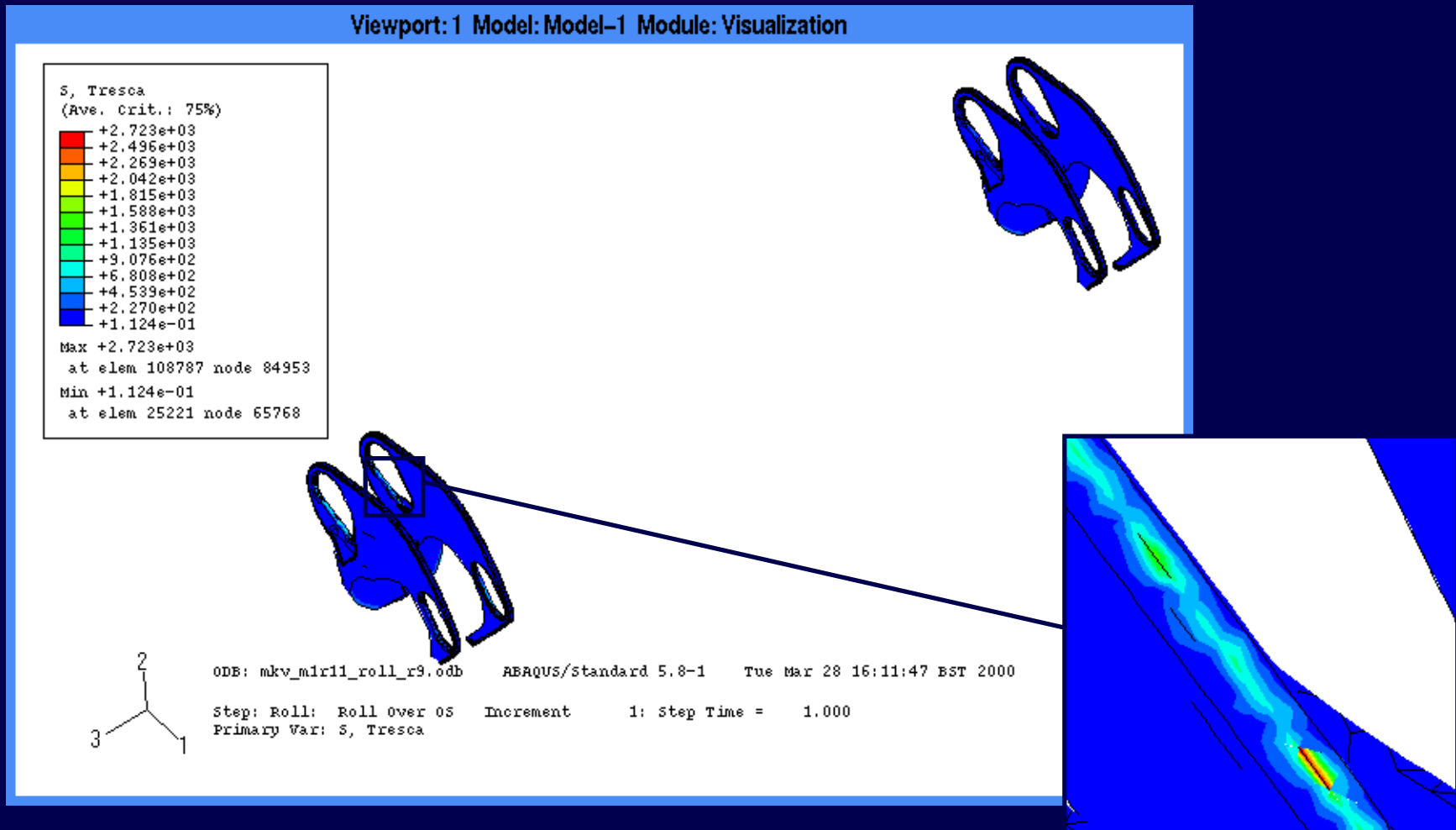


# Stress Analysis - Results



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## ■ Rollover LH - Side Plate - TRESCA Stress



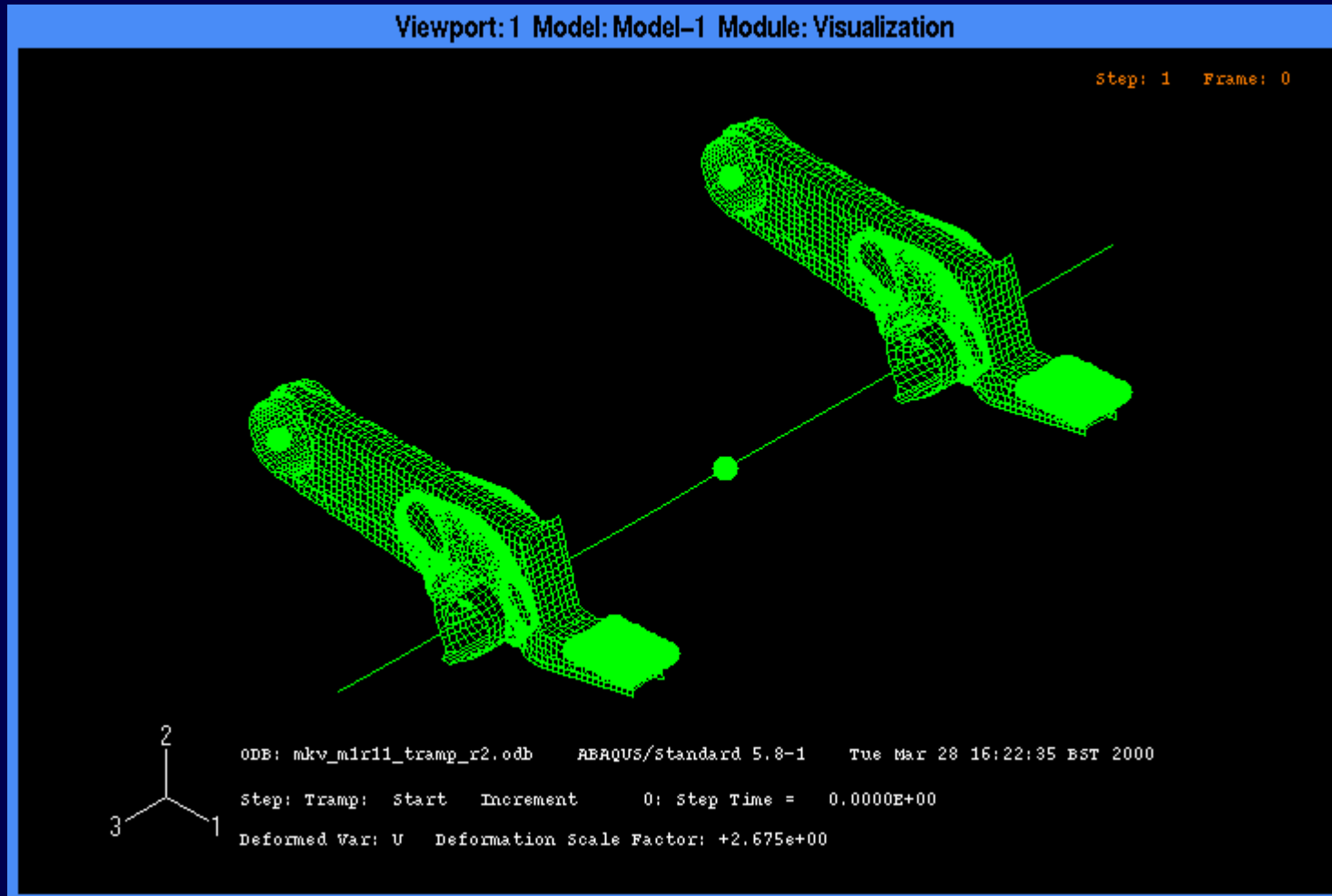
## **Loadcase 2: Tramp Manoeuvre**

# Stress Analysis - Results



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## ■ Tramp Manoeuvre - Displaced Shape

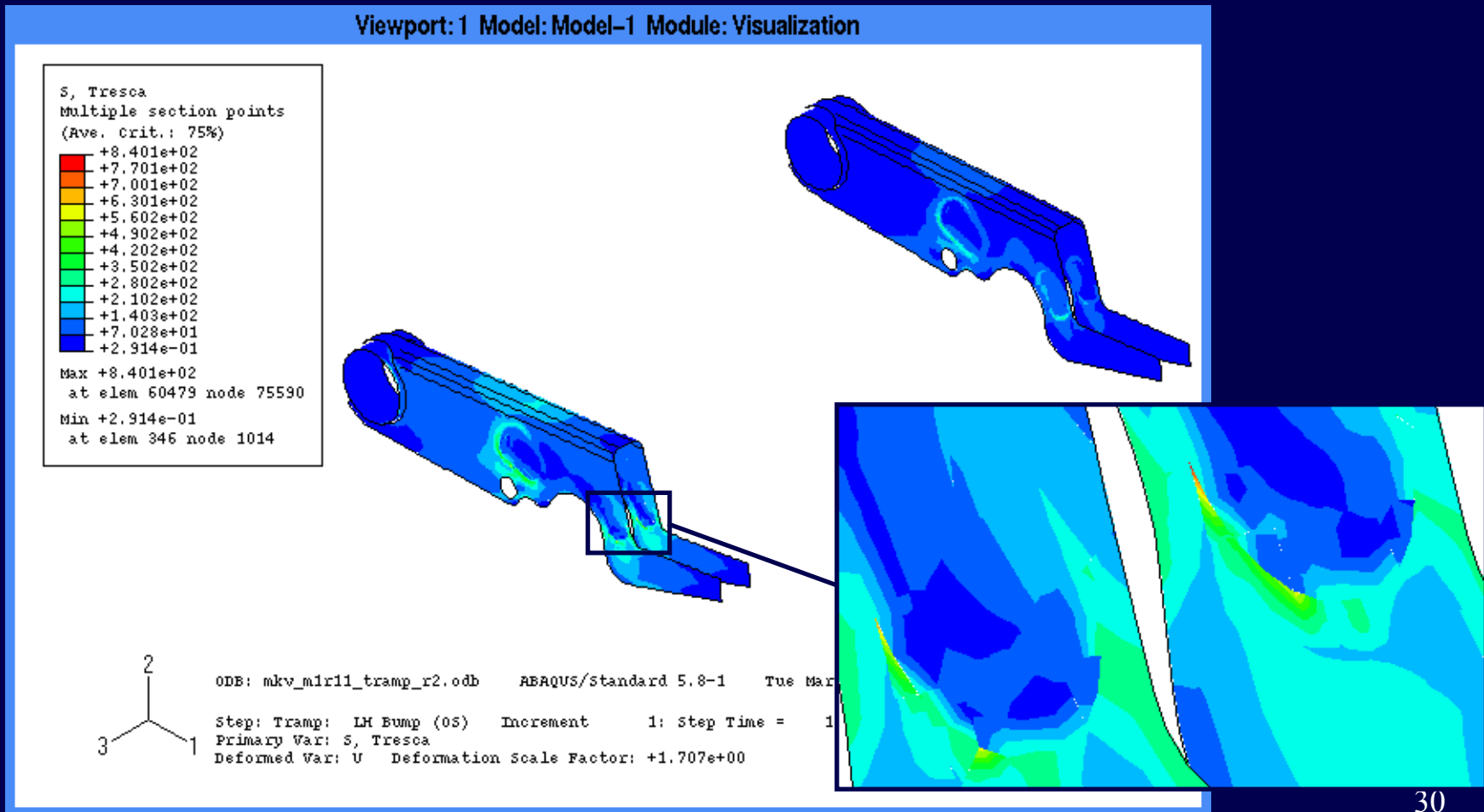


# Stress Analysis - Results



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## ■ Tramp LH/RH Bump - Arm/Pivot - TRESCA Stress

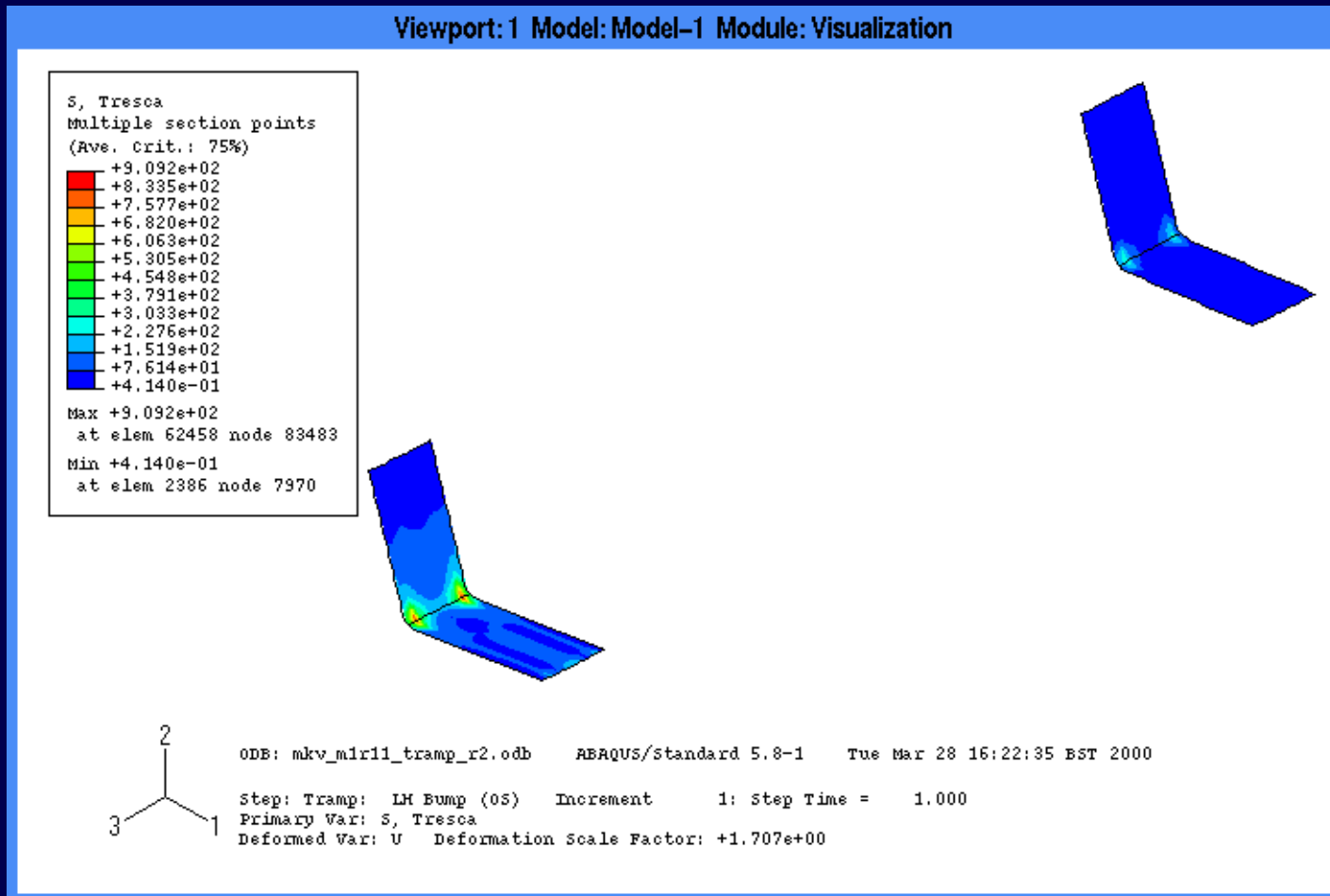


# Stress Analysis - Results



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## ■ Tramp LH/RH Bump - Spring Platform - TRESCA Stress

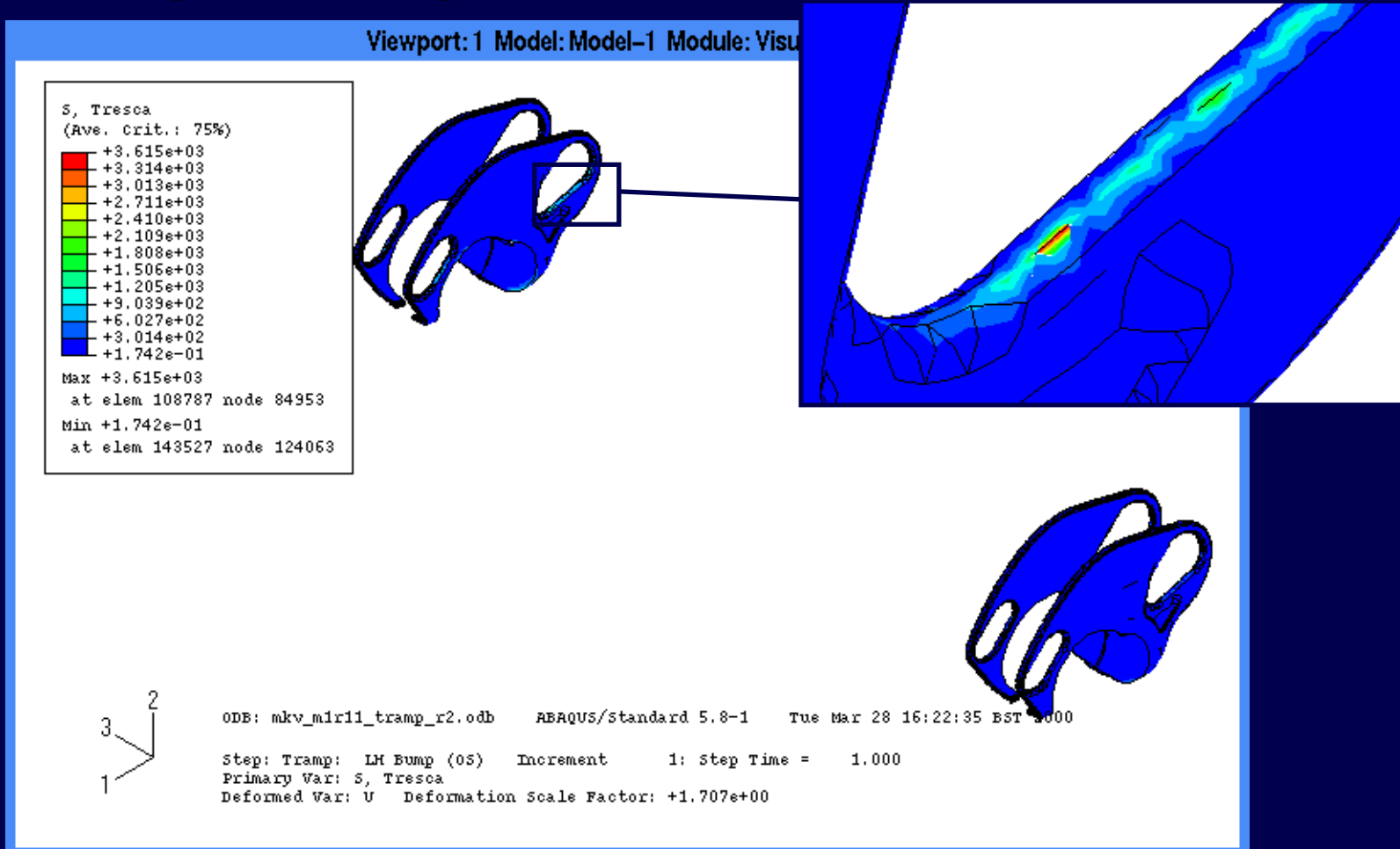


# Stress Analysis - Results



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## ■ Tramp LH/RH Bump - Side Plate - TRESCA Stress







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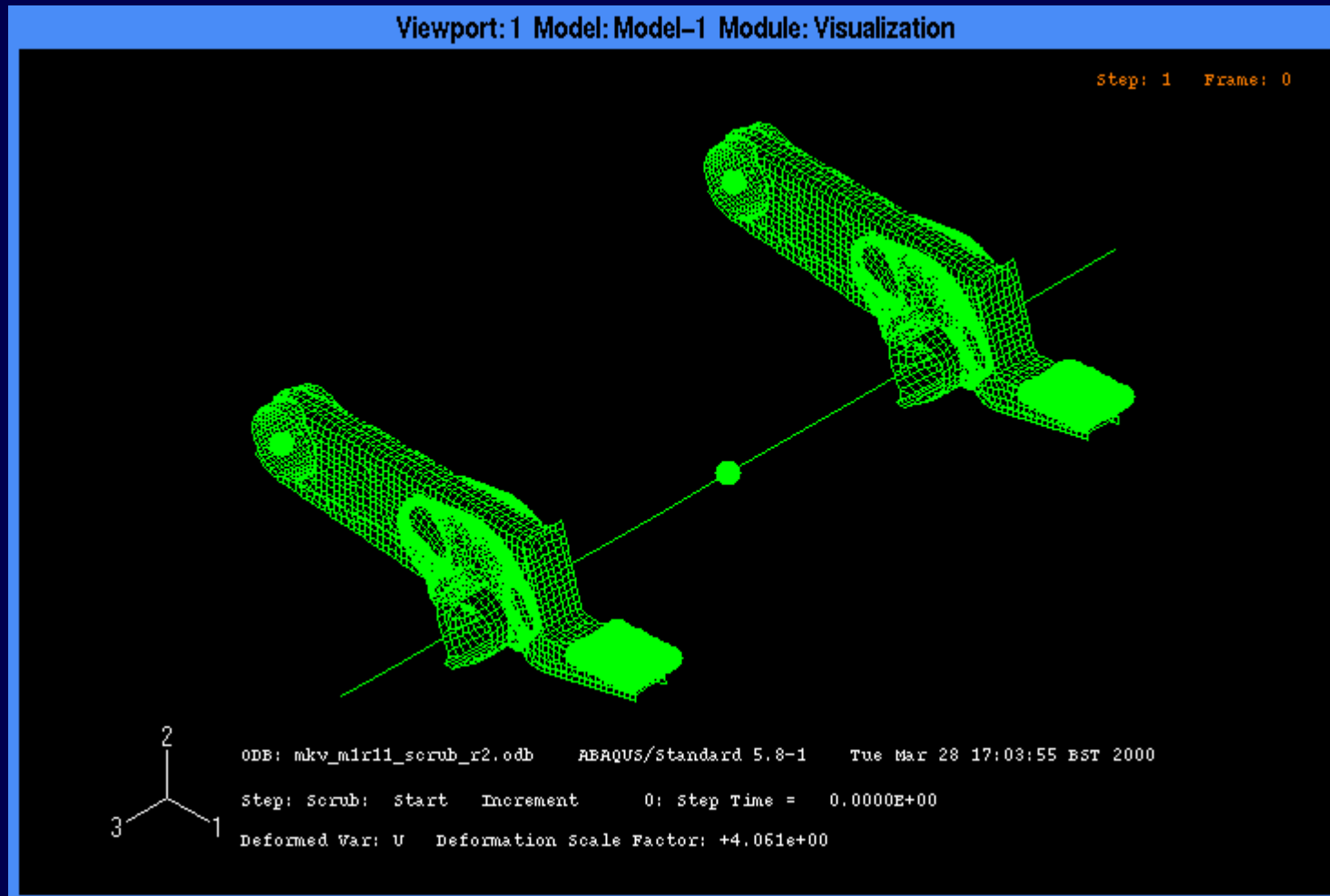
## **Loadcase 3: Scrub Manoeuvre**

# Stress Analysis - Results



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## ■ Scrub Manoeuvre - Displaced Shape

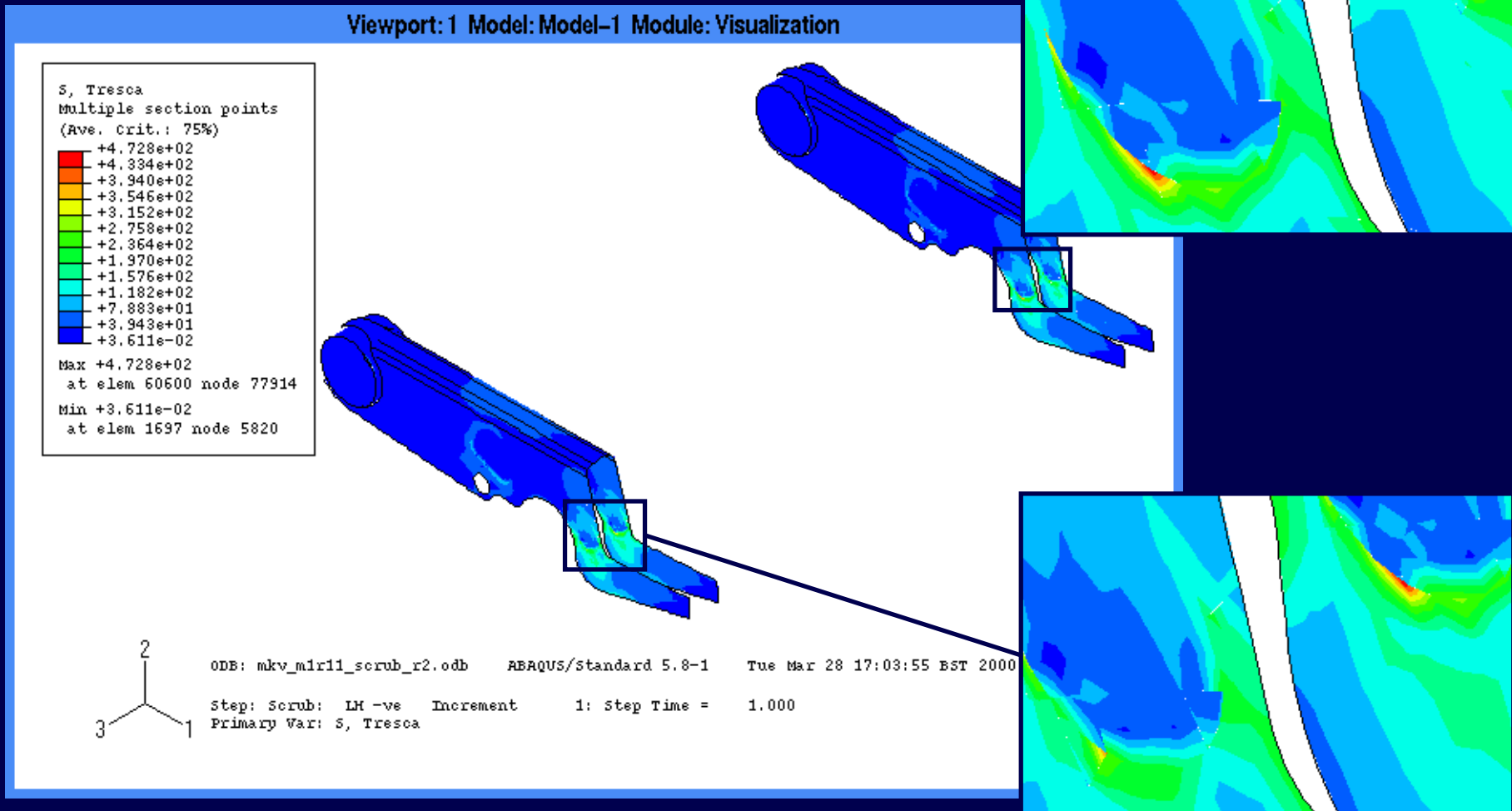


# Stress Analysis - Results



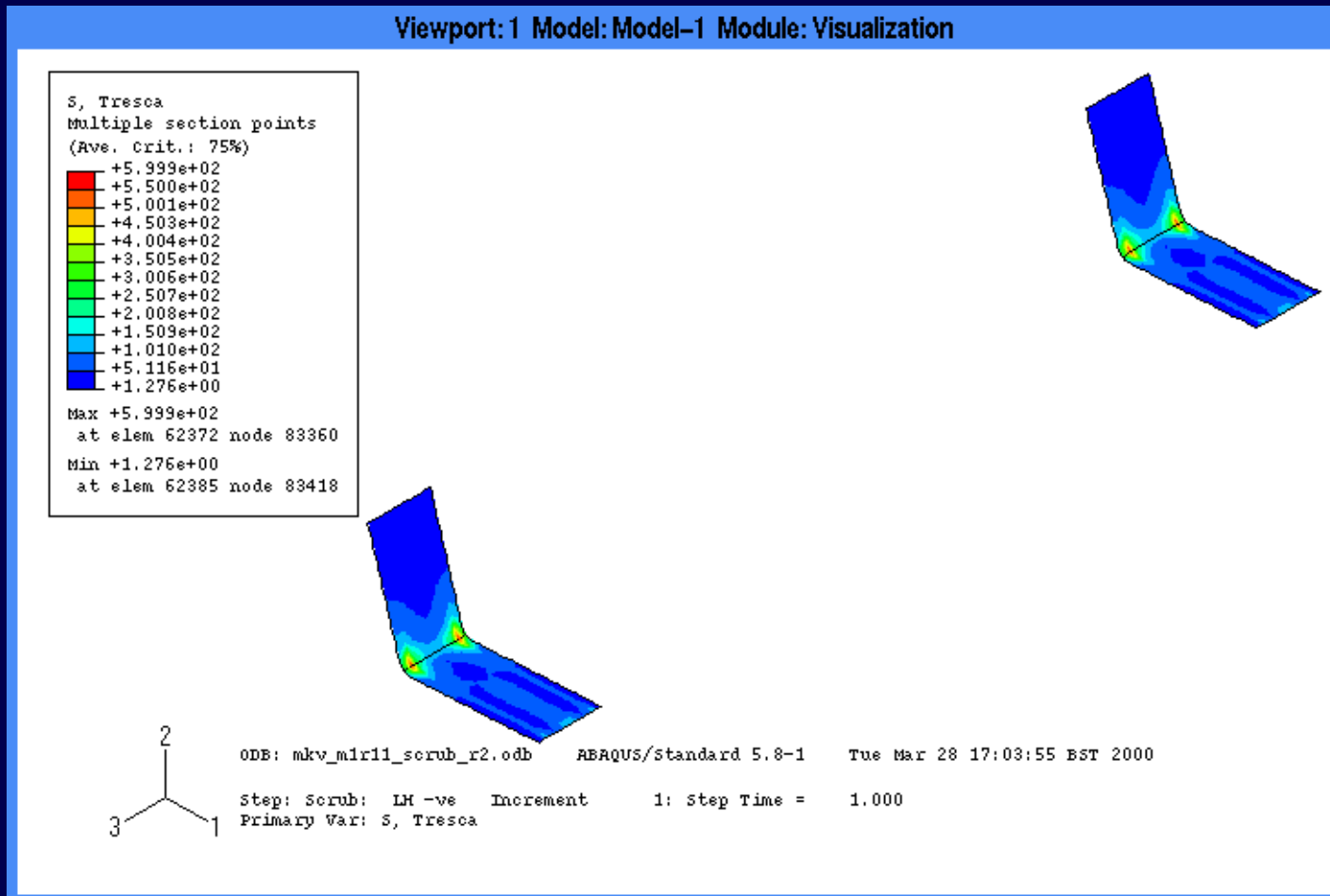
Adding value through knowledge

## ■ Scrub LH -ve - Arm/Pivot - TRESCA Stress



# Stress Analysis - Results

## ■ Scrub LH -ve - Spring Platform - TRESCA Stress

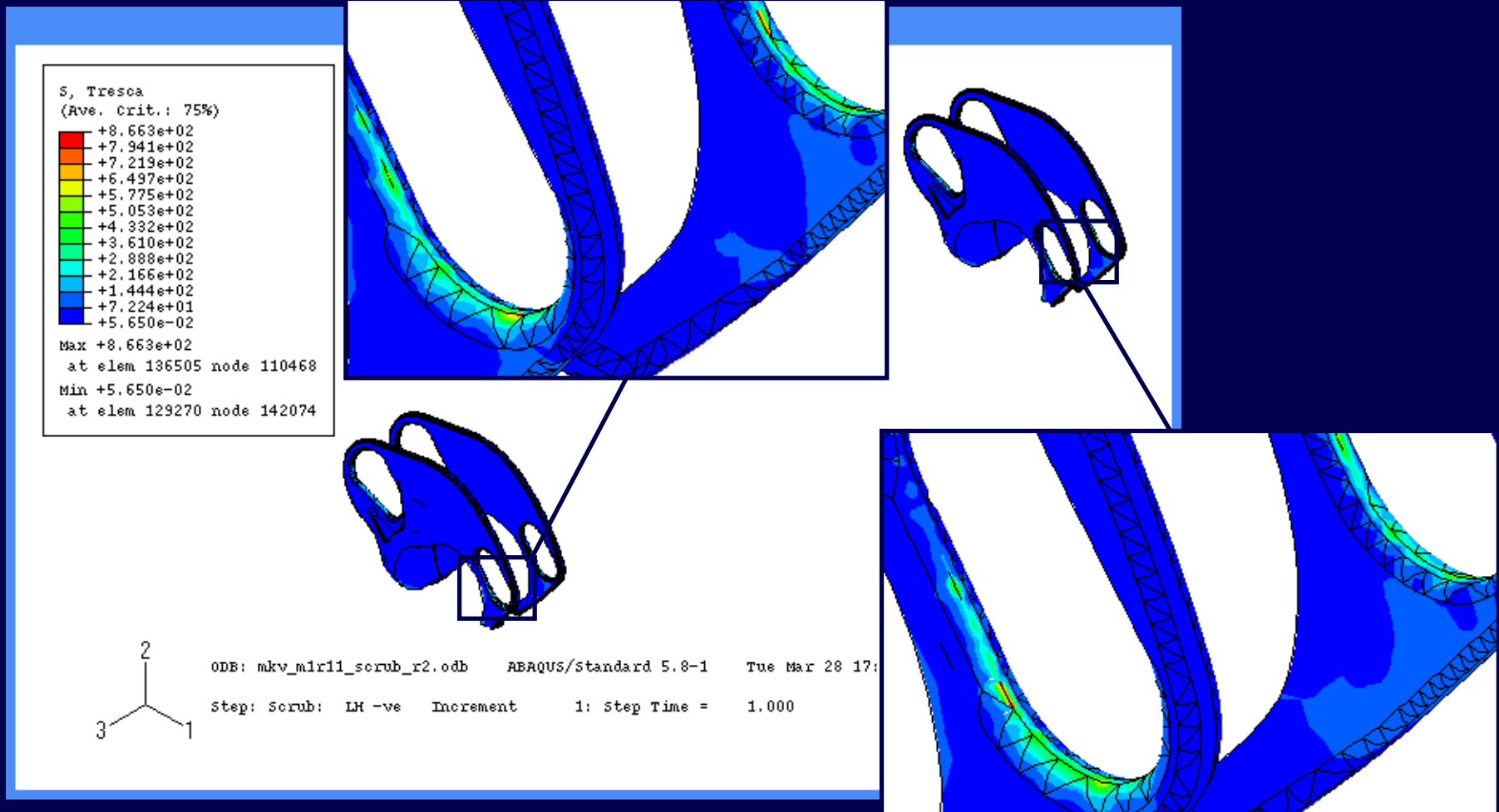


# Stress Analysis - Results



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## ■ Scrub LH -ve - Side Plate - TRESCA Stress



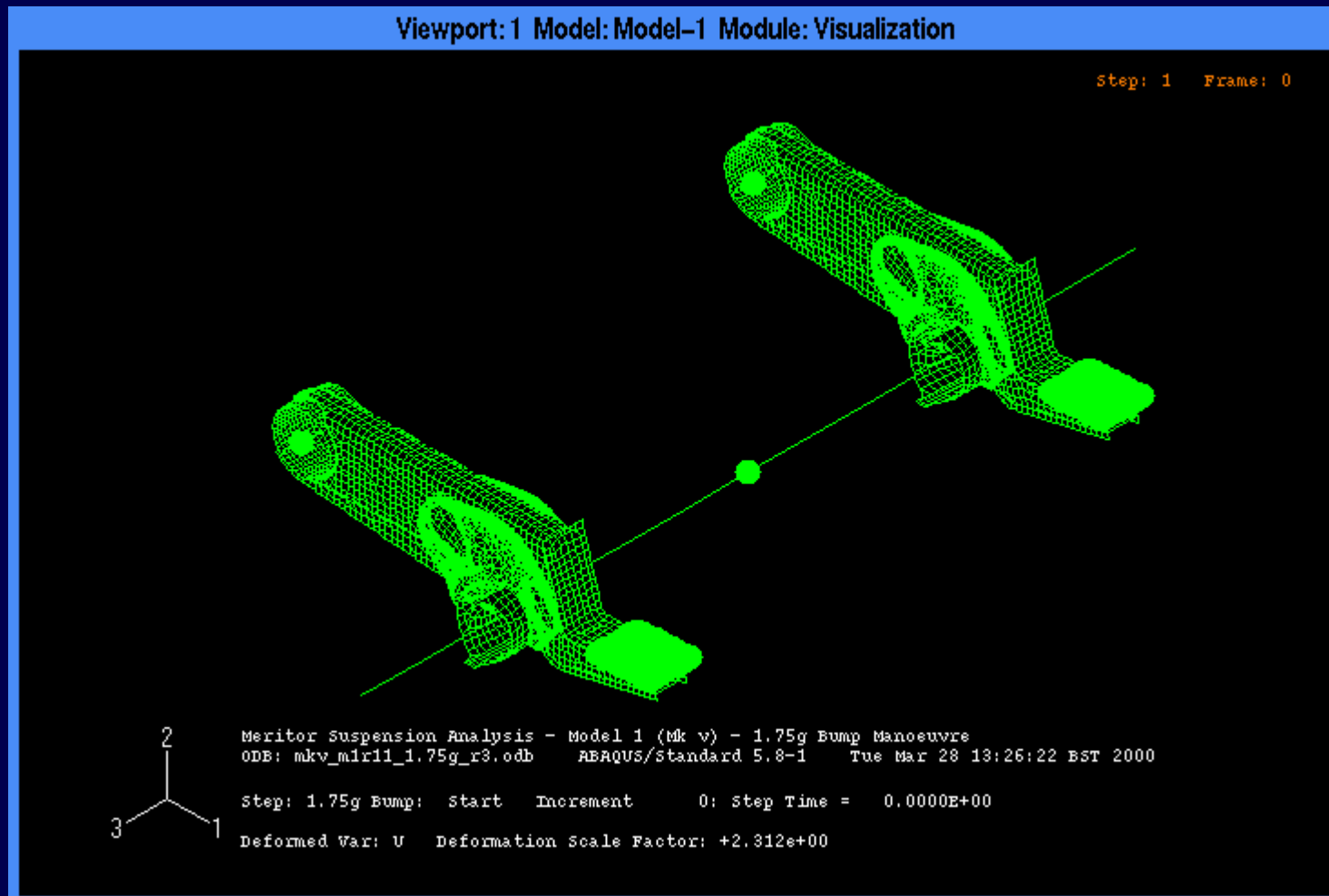
## **Loadcase 4: 1.75g Bump Manoeuvre**

# Stress Analysis - Results



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## ■ 1.75g Bump Manoeuvre - Displaced Shape



# Stress Analysis - Results

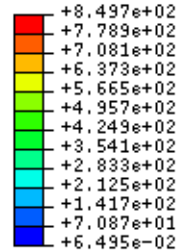


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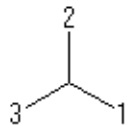
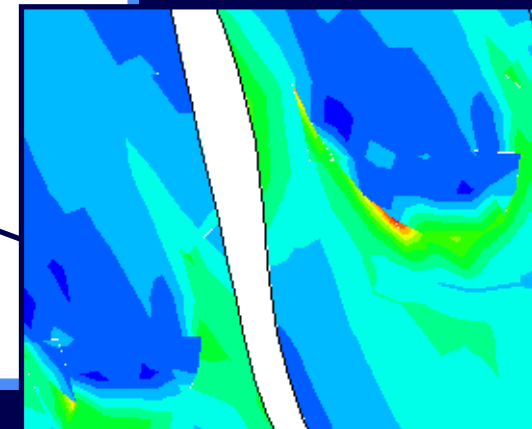
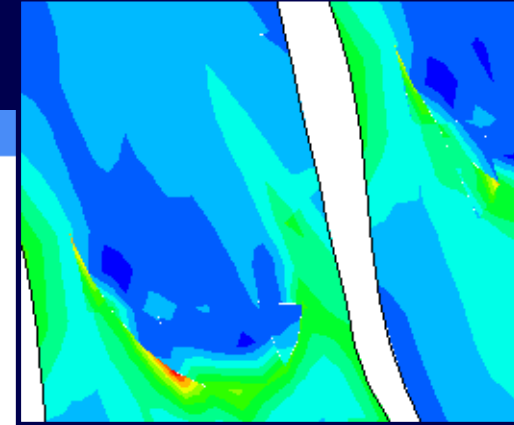
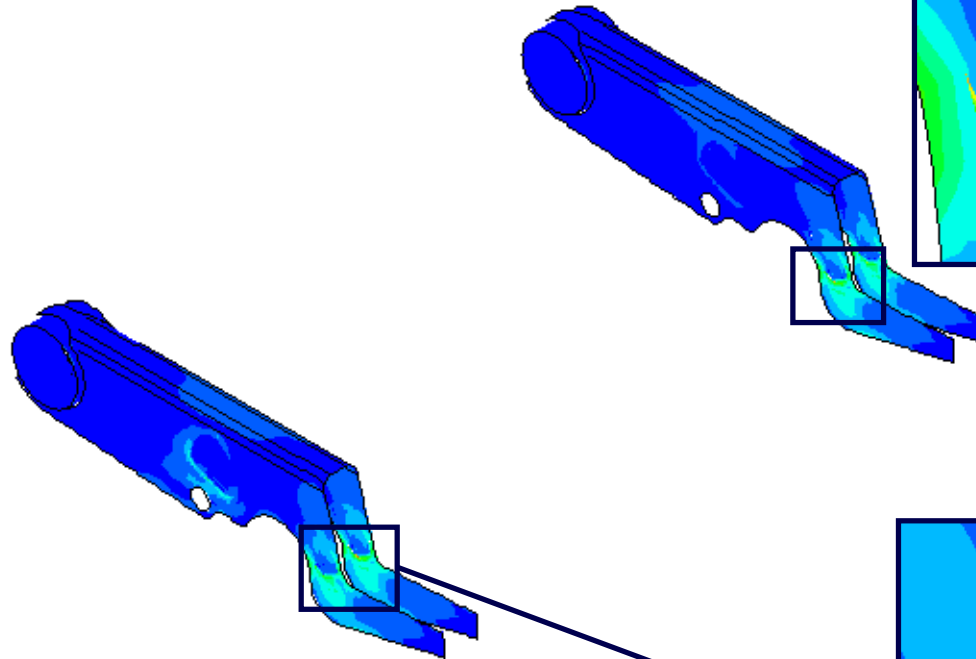
## 1.75g Bump - Arm/Pivot - TRESCA Stress

Viewport: 1 Model: Model-1 Module: Visualization

S, Tresca  
Multiple section points  
(Ave. Crit.: 75%)



Max +8.497e+02  
at elem 60600 node 77914  
Min +6.495e-02  
at elem 61697 node 81305



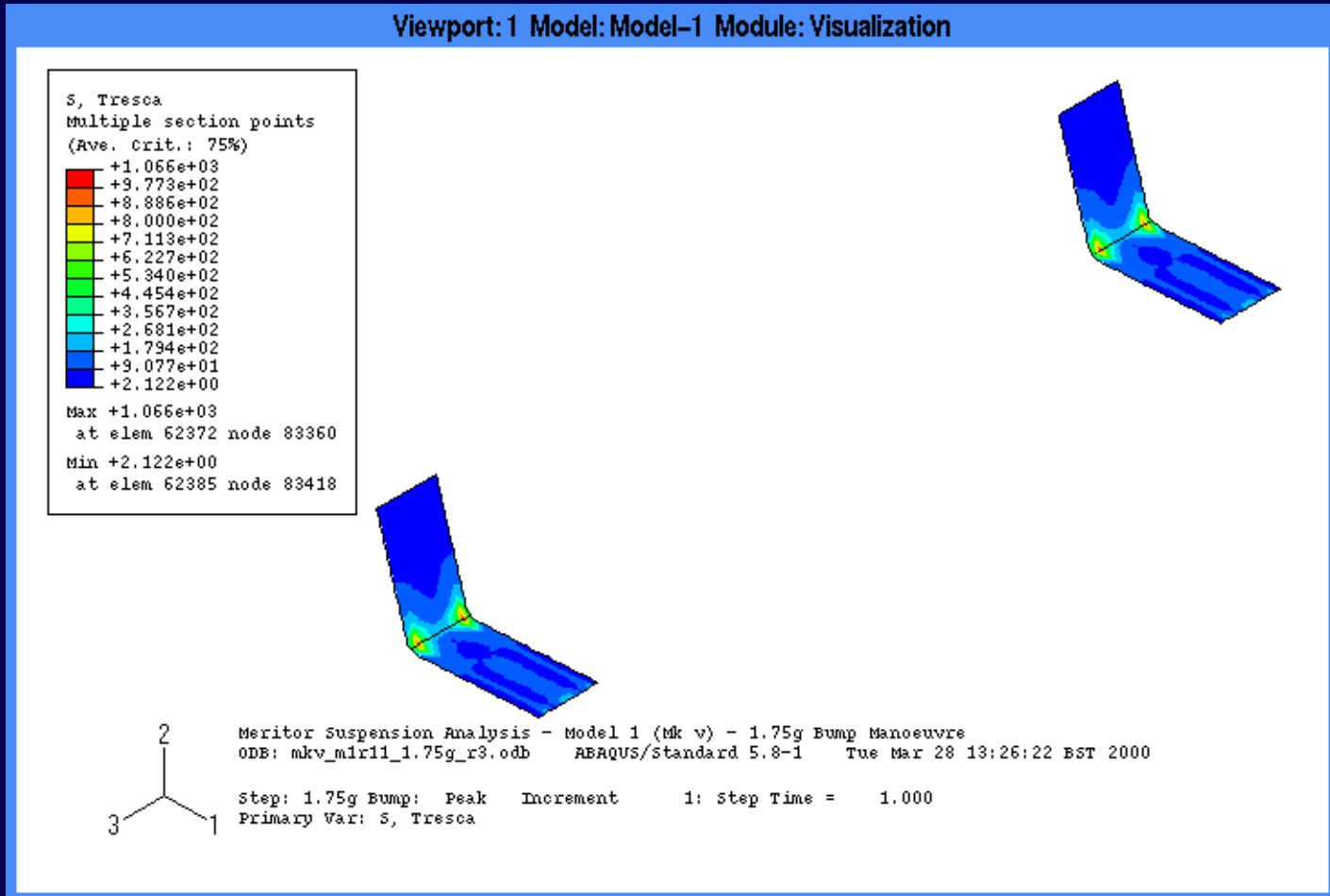
Meritor Suspension Analysis - Model 1 (mk v) - 1.75g Bump Manoeuvre  
ODB: mkv\_mlr11\_1.75g\_r3.odb ABAQUS/standard 5.8-1 Tue Mar 28 13:26:22 BST 2000

Step: 1.75g Bump: Peak Increment 1: Step Time = 1.000  
Primary Var: S, Tresca



# Stress Analysis - Results

## 1.75g Bump - Spring Platform - TRESCA Stress

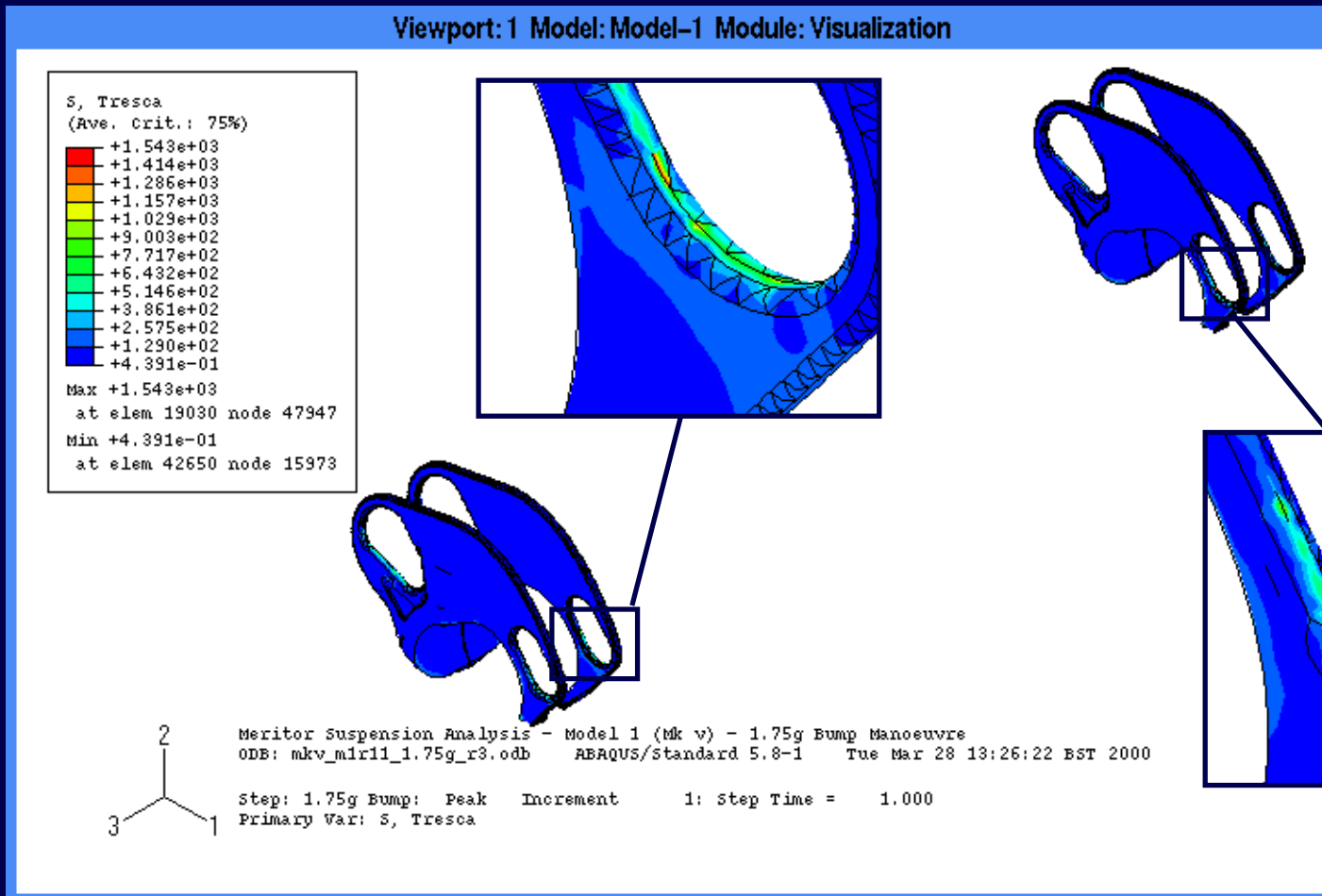


# Stress Analysis - Results



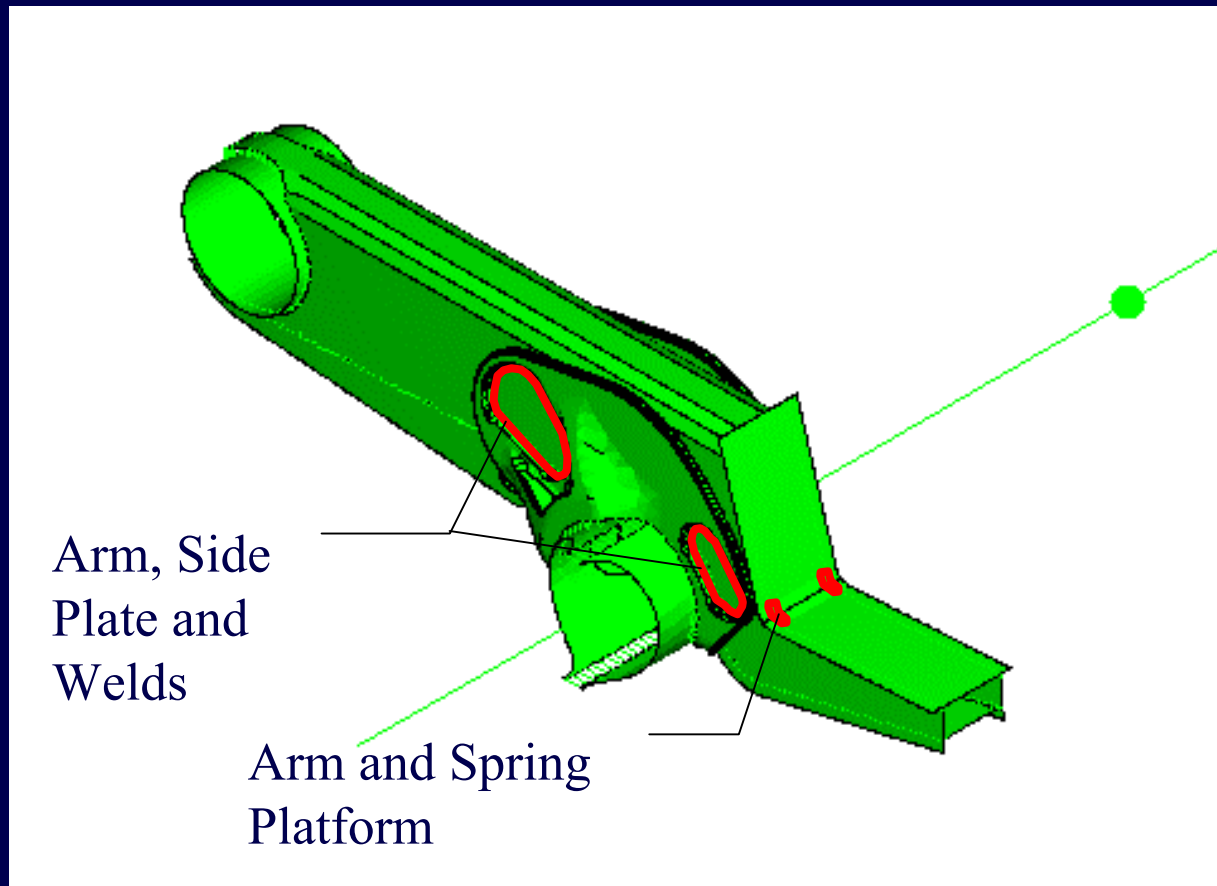
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## 1.75g Bump - Side Plate - TRESCA Stress



# Stress Analysis - Results

- **Critical Locations of Peak Stresses**





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# Assessment

Three failure mechanisms are relevant :-

- **Crack initiation**
  - Fatigue assessment using BS5400 rules
- **Crack Propagation**
  - Fracture mechanics using R6 procedure
- **Cyclic plasticity causing incremental collapse**
  - Shakedown criteria

- **Parent Material and Welds**
  - **BS5400 Part 10 & BS7608**
  - **Critical sample stress locations assessed**
  - **Alternating stress calculated using FORTRAN programme**
  - **Predicted number of cycles to failure calculated**

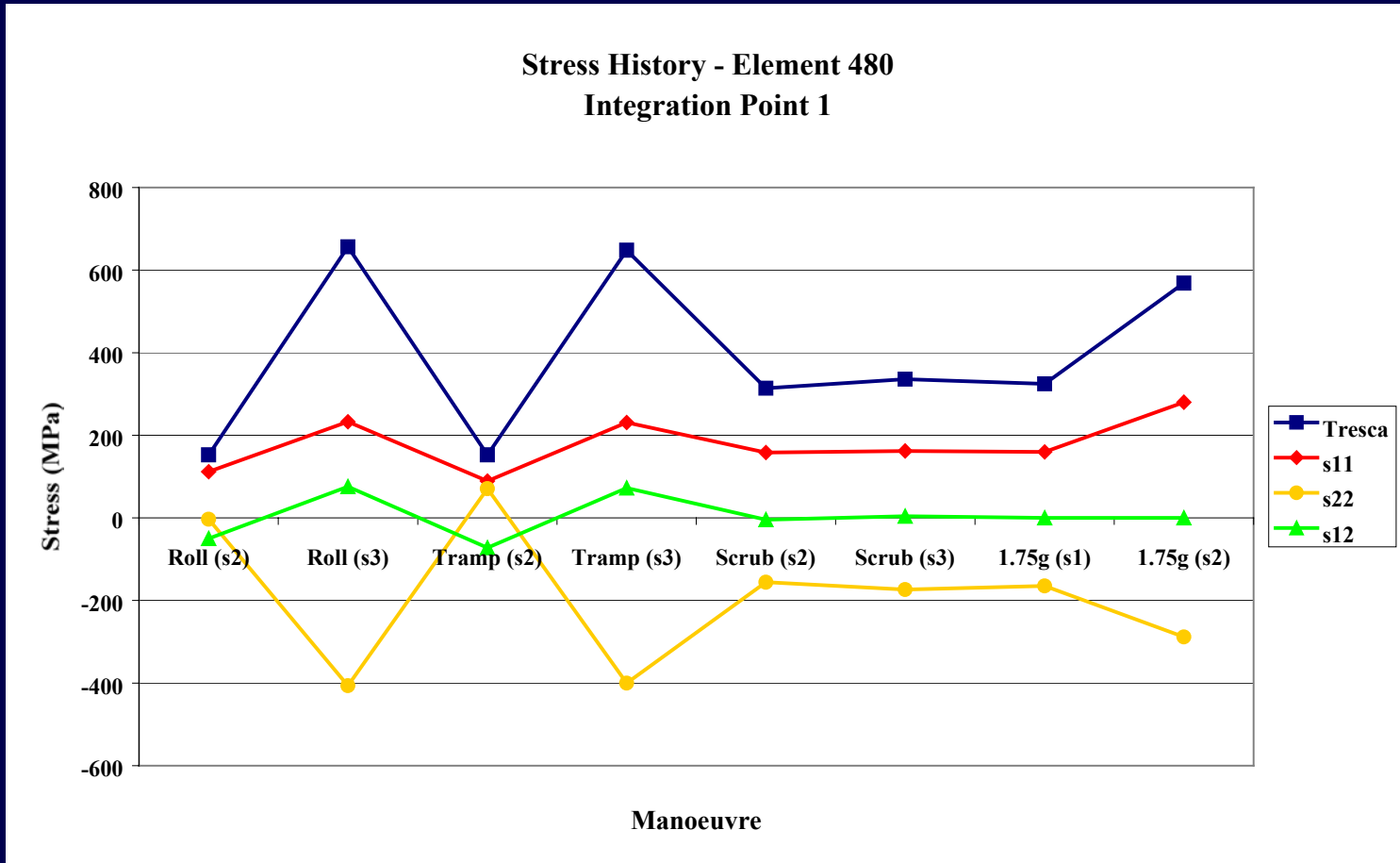


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# **Fatigue Assessment of Parent Material**

# Assessment - Stress History

## ■ Example of Stress Range Selection





# Fatigue Assessment - Results



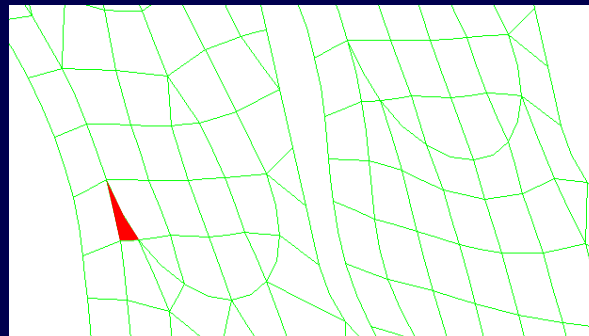
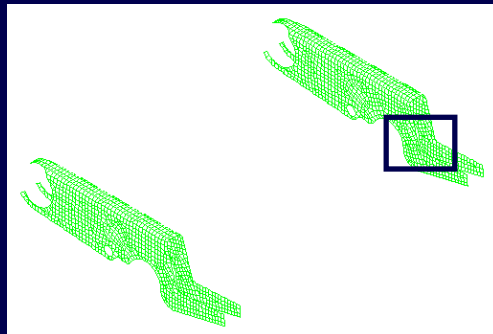
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## ■ Arm - Element 480

| Manoeuvre | Detail Class | Alternating Stress (MPa) | Stress Range (MPa) | Predicted Cycles to Failure (N) | Usage              |
|-----------|--------------|--------------------------|--------------------|---------------------------------|--------------------|
| Roll      | W (G)        | 290                      | 580                | 1.9e3 (2.9e3)                   | <b>16.8 (11.0)</b> |
| Tramp     | W (G)        | 339                      | 678                | 1.2e3 (1.8e3)                   | <b>26.7 (17.5)</b> |
| Scrub     | W (G)        | 14                       | 28                 | 1.6e7 (2.6e7)                   | <b>0.0 (0.0)</b>   |
| 1.75g     | W (G)        | 122                      | 244                | 2.5e4 (3.9e4)                   | <b>1.3 (0.8)</b>   |

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Σ **44.8 (29.3)**

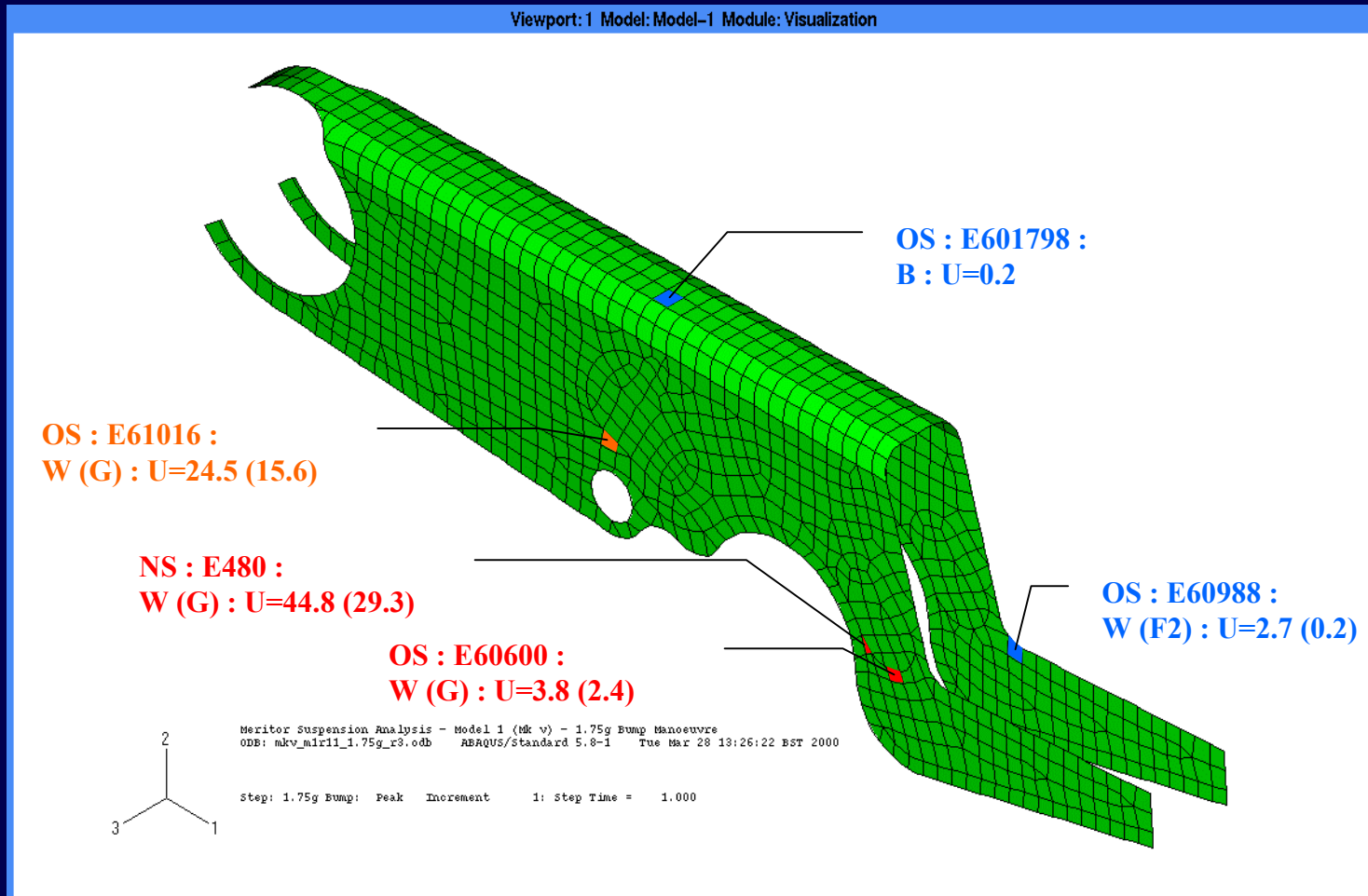


# Fatigue Assessment - Results



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## ■ Arm - Fatigue Usage

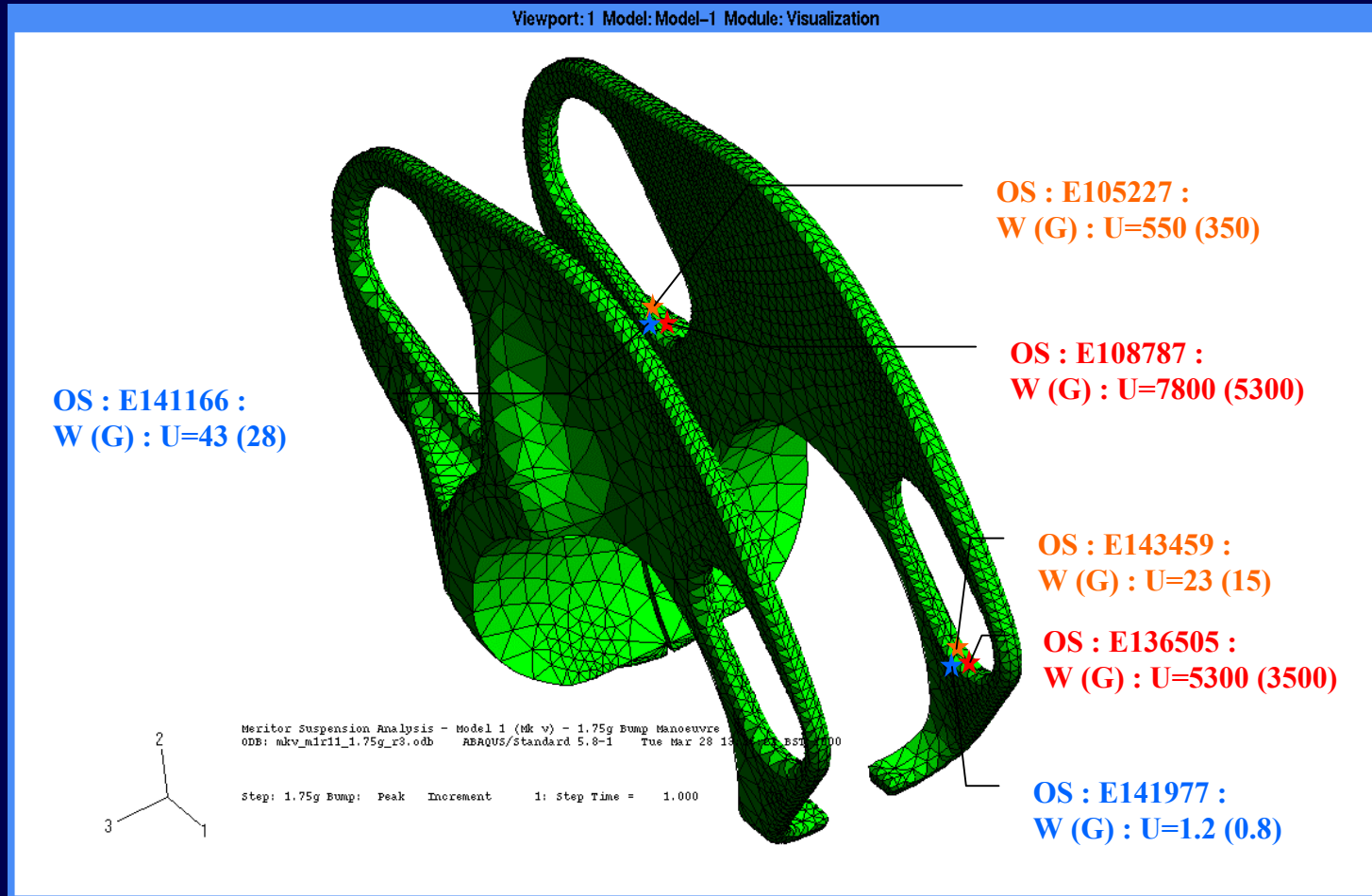


# Fatigue Assessment - Results

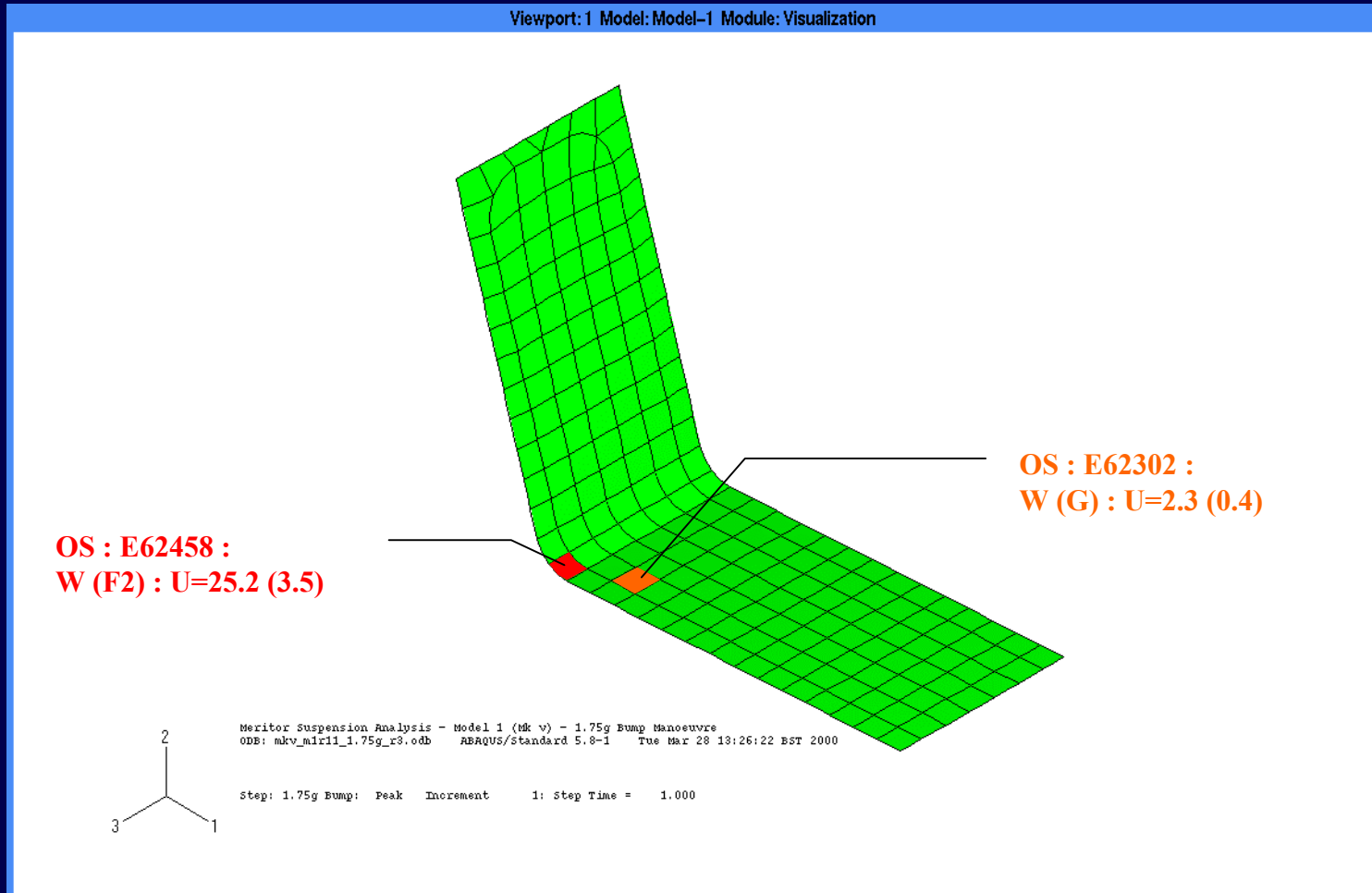


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## ■ Arm - Fatigue Usage



## ■ Spring Platform - Fatigue Usage





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# **Fatigue Assessment of Welds**

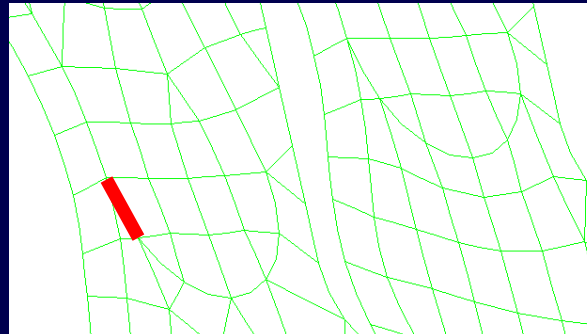
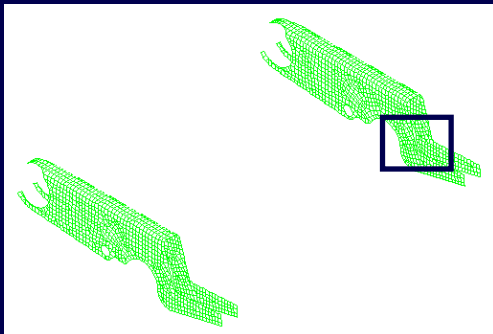
# Fatigue Assessment of Welds



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## ■ Plug Weld Adjacent Element 480 (Arm side of weld only)

| Manoeuvre | Detail Class | Alternating Stress (MPa) | Stress Range (MPa) | Predicted Cycles to Failure (N) | Usage      |
|-----------|--------------|--------------------------|--------------------|---------------------------------|------------|
| Roll      | W            | 137                      | 273                | 1.8e4                           | <b>1.8</b> |
| Tramp     | W            | 132                      | 263                | 2.0e4                           | <b>1.6</b> |
| Scrub     | W            | 6                        | 12                 | 2.1e8                           | <b>0.0</b> |
| 1.75g     | W            | 67                       | 133                | 1.6e5                           | <b>0.2</b> |




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Σ **3.6**



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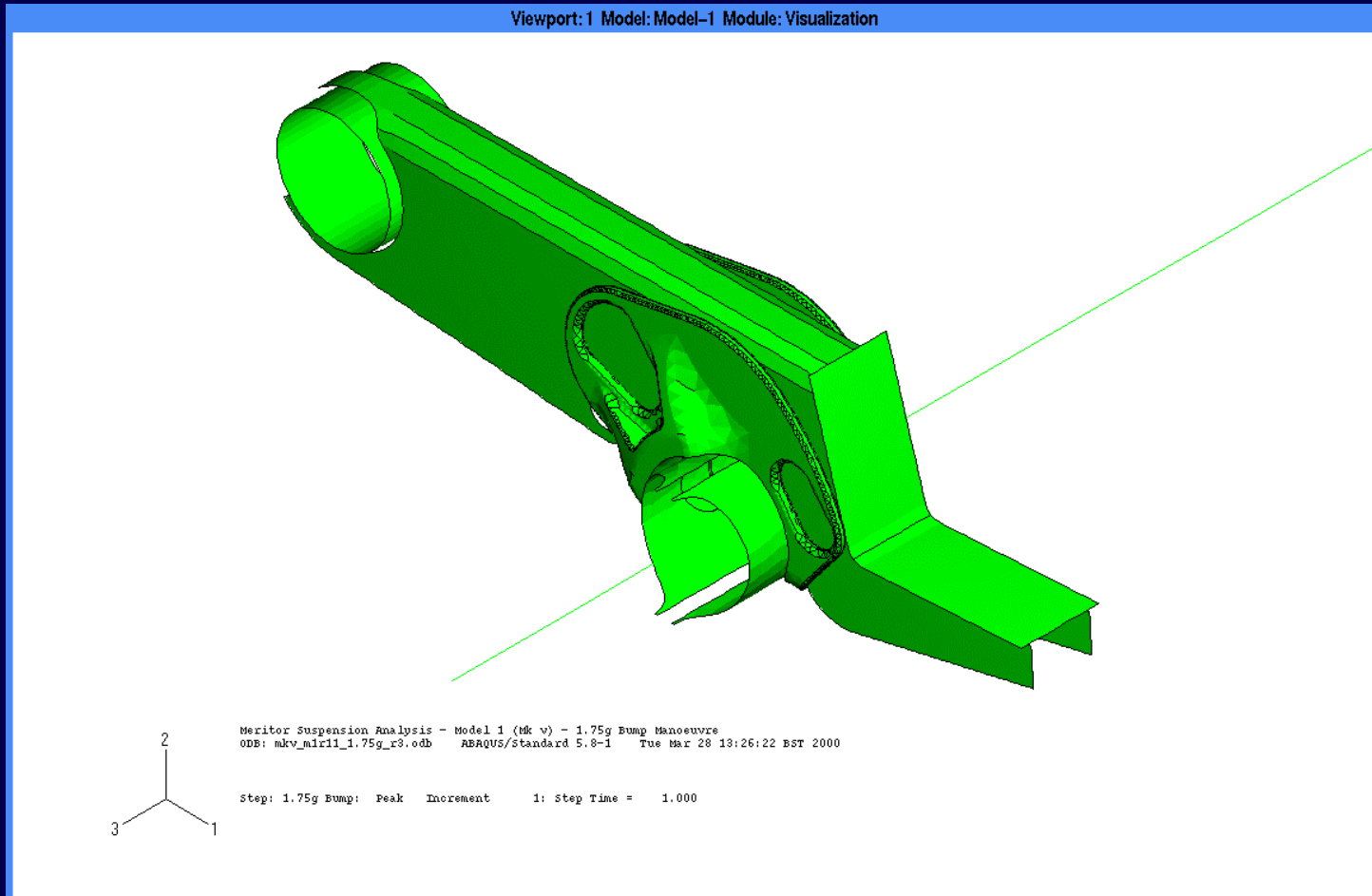
# Why Fatigue Failure?

# Why Fatigue Failure?



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## ■ Load Path



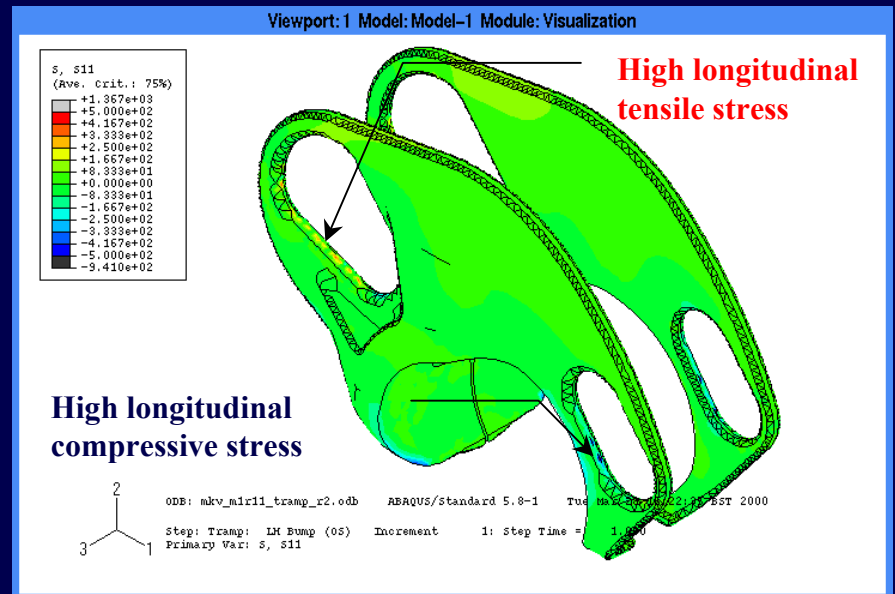
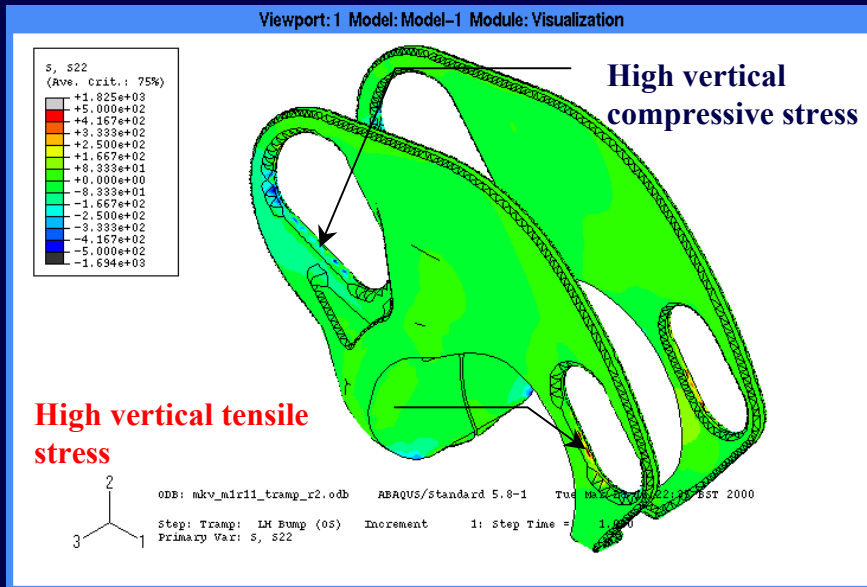


# Why Fatigue Failure?



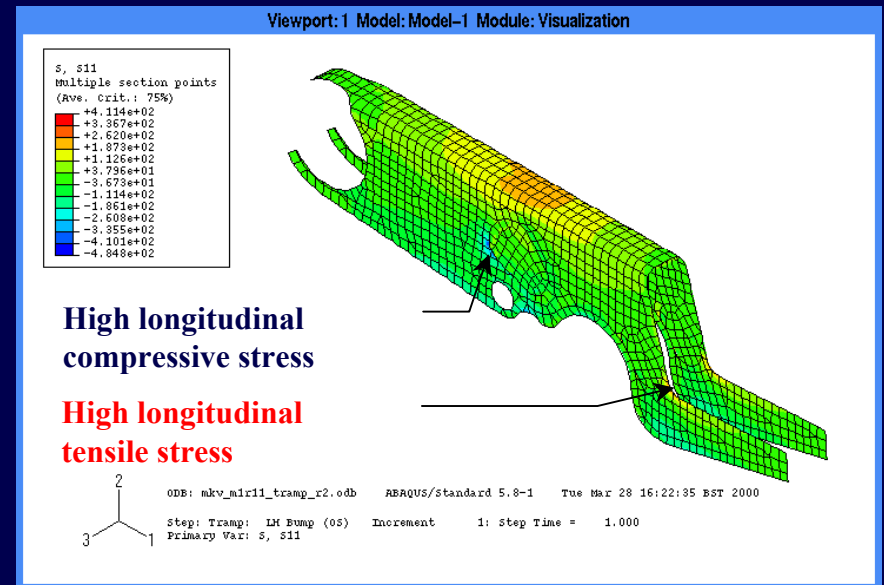
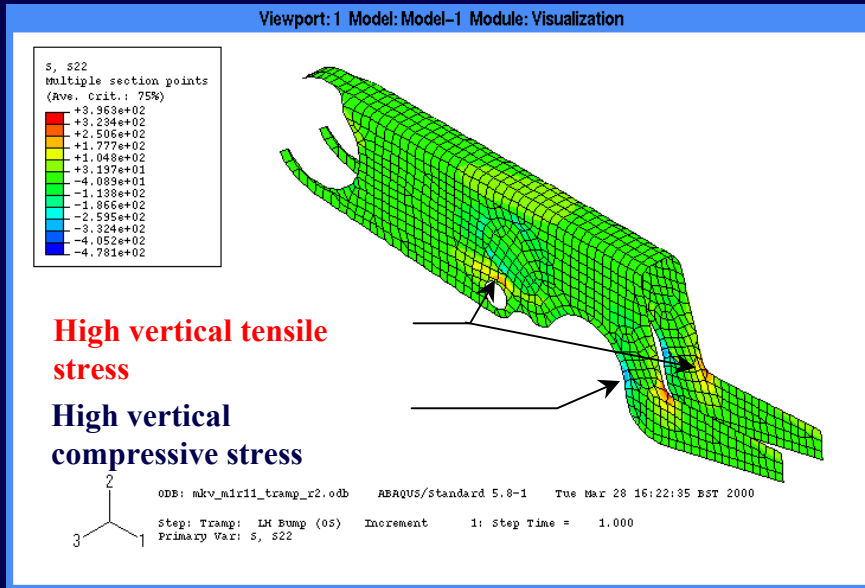
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- Large stresses from side plate to arm



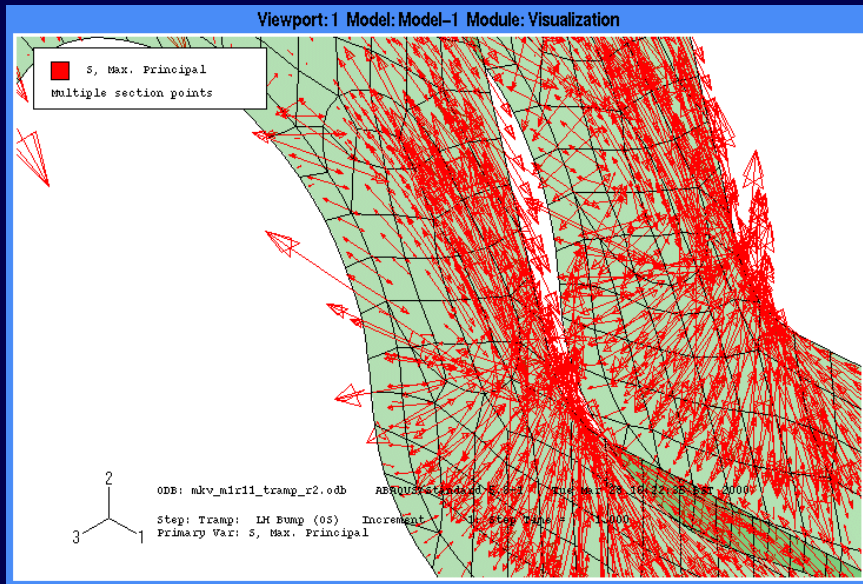
# Why Fatigue Failure?

## ■ Action of plug welds on arm

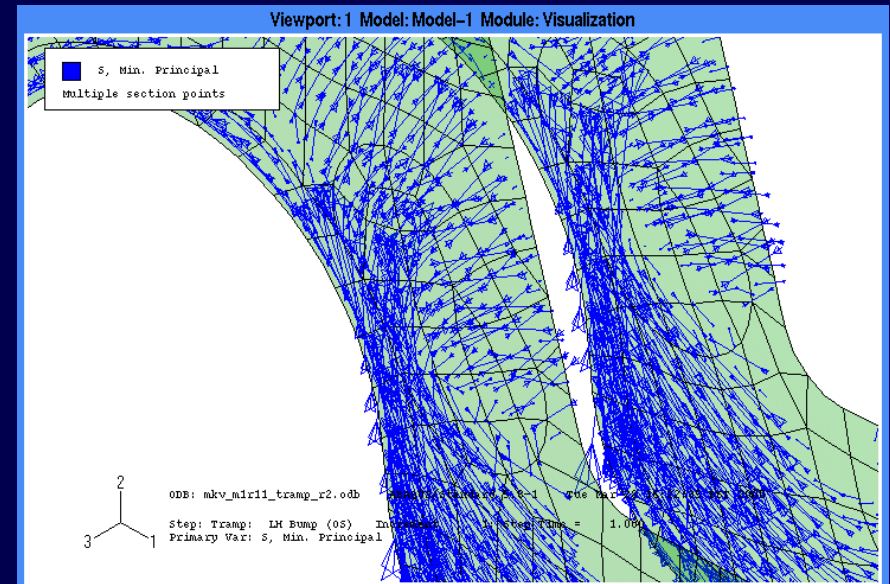


# Why Fatigue Failure?

- Stress flow dictated by
  - loading mechanism
  - Shape and location of the plug welds



Max. Principal Stress (tension)

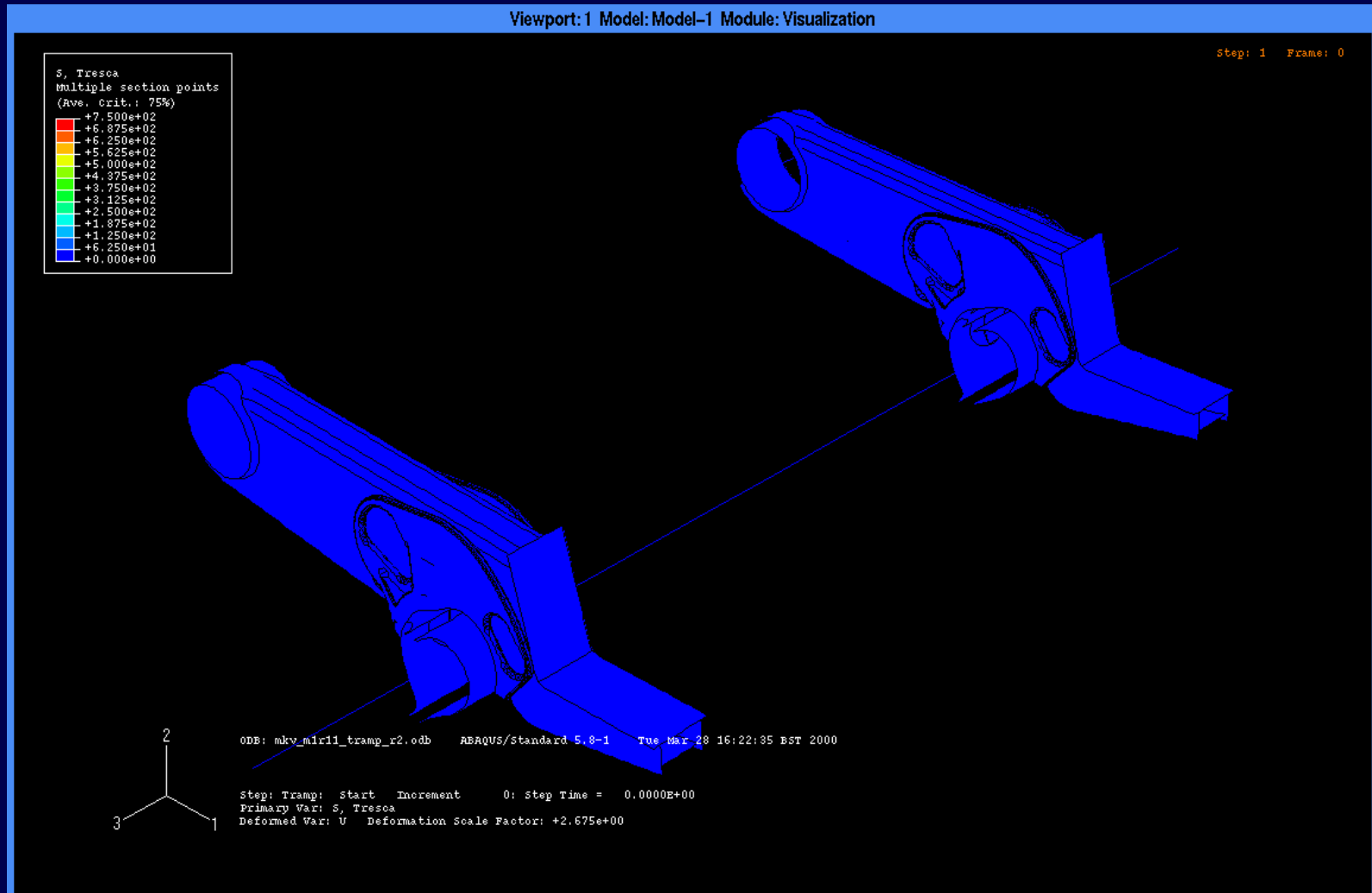


Min. Principal Stress (comp.)

# Why Fatigue Failure?

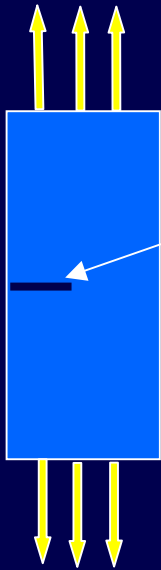


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# Fracture Mechanics

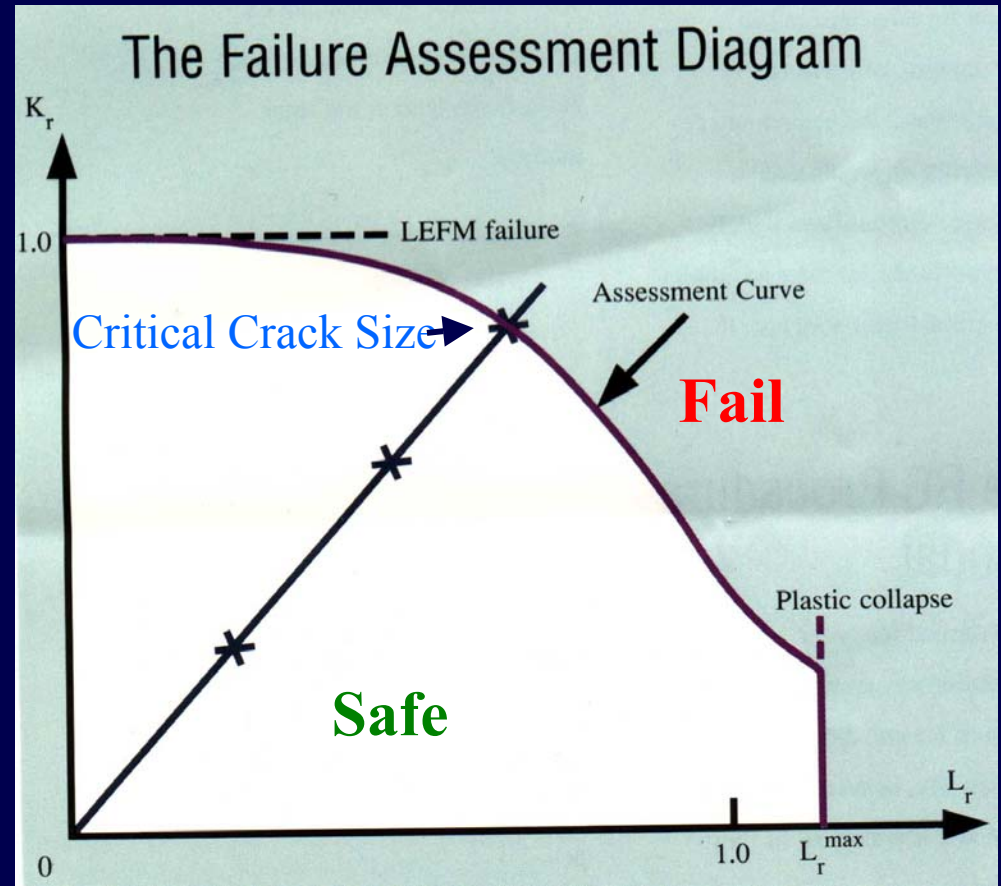
R6 used to calculate the critical crack size



Stress intensity,  $K_I$

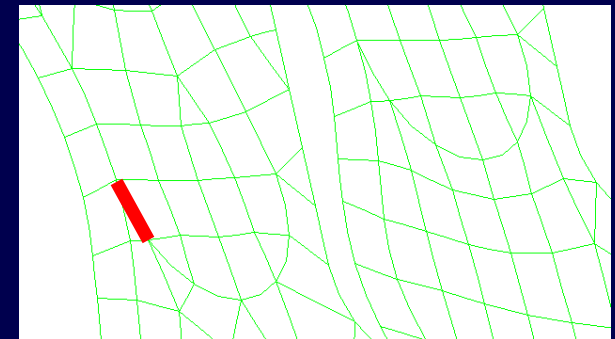
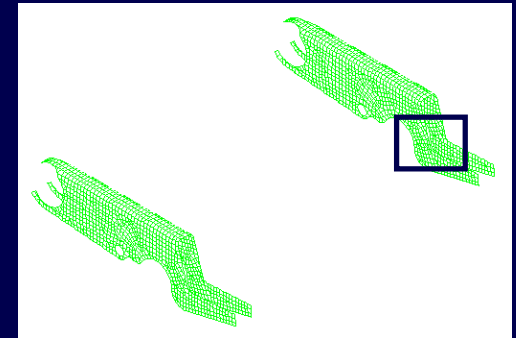
Failure if  $K_I > K_{IC}$

$$K_r = K_I / K_{IC}$$



■ Crack Propagation in Arm for Element 480 (top surface)  
Vertical (s22) stress assessment

| Manoeuvre | Critical Crack Size (mm) | Crack Growth over 32000 cycles (mm) | Initial Crack Size to Cause Failure (mm) |
|-----------|--------------------------|-------------------------------------|--|
| Roll      | 3.5                      | 1.9                                 | 1.7                                      |
| Tramp     | 3.6                      | 1.8                                 | 1.8                                      |
| Scrub     | 4.4                      | 0.1                                 | 4.3                                      |
| 1.75g     | 3.9                      | 0.6                                 | 3.3                                      |





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# Conclusions

- **Geometric data**
  - **Transfer from CAD to FE works**
  - **Provision of shell geometry as mid-surfaces and solid as volume**
- **Stress Analysis**
  - **Full test simulation possible**
  - **Peak stresses identified**
  - **Loading mechanism and stress flow understood**

**cont'd.**



## ■ Assessment

- **Vertical loading dominant**
- **Fatigue failure in parent metal and in welds**
- **Allowable stress range ~226MPa for 32,000 cycles for detail class W**
- **Local stress concentrations cause failures**
- **Roll and Tramp manoeuvres cause most damage**
- **Accelerated fatigue testing by using high loads causes plasticity and incremental collapse**
- **Functional failure occurs when theoretical fatigue usage factor is 15 or more**



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# Recommendations

## Simulation

- **Include bracket at the pivoted end for more realistic test simulation**
- **Conduct non-linear analysis of the**
  - **air-spring**
  - **bush**

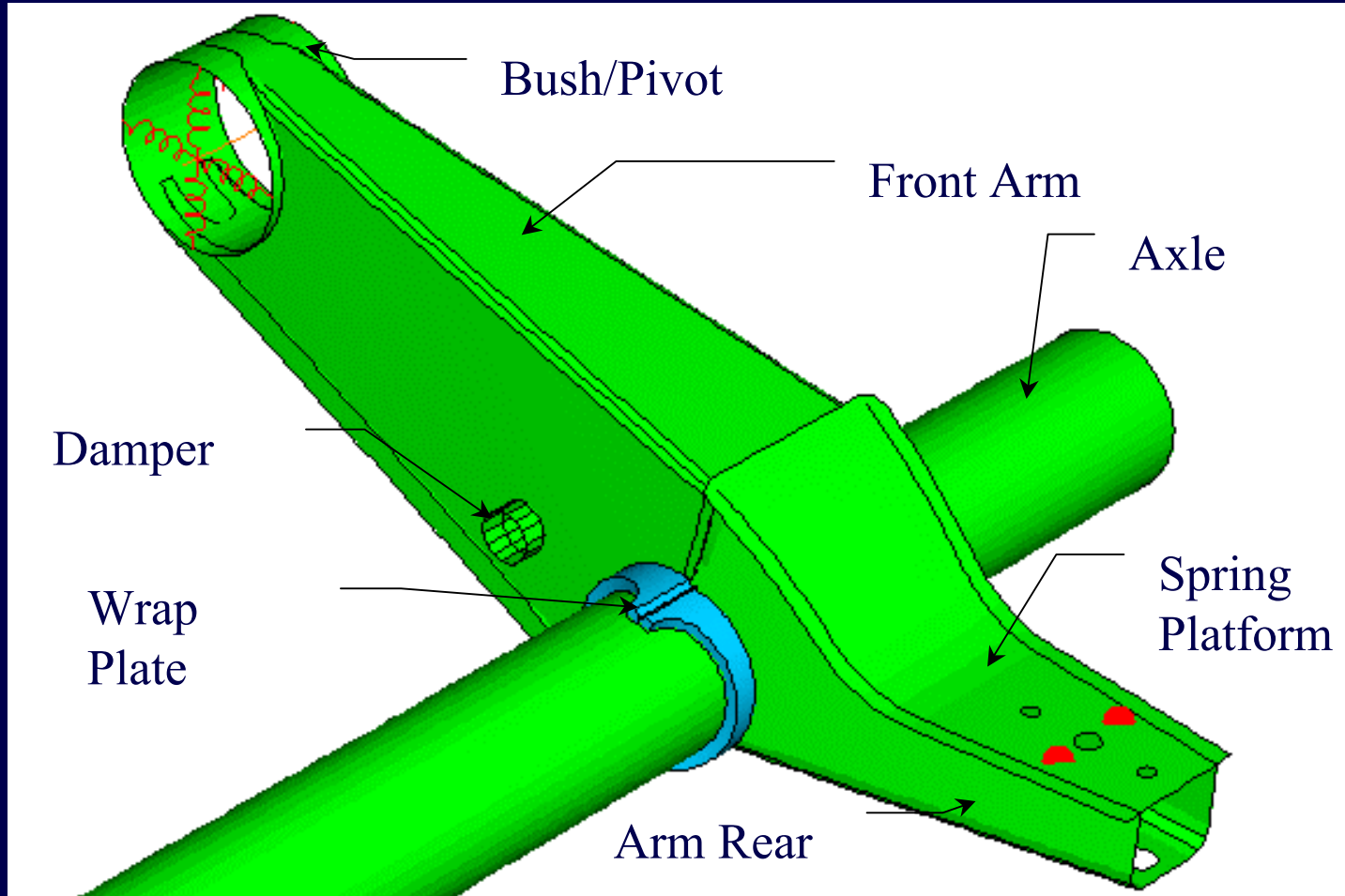
## Design

- **Redesign the plug weld connection to avoid peak stresses in the lower regions**
- **Investigate spring platform local strengthening**
- **Remove the Cover Plate**

# New Design without Side Plate



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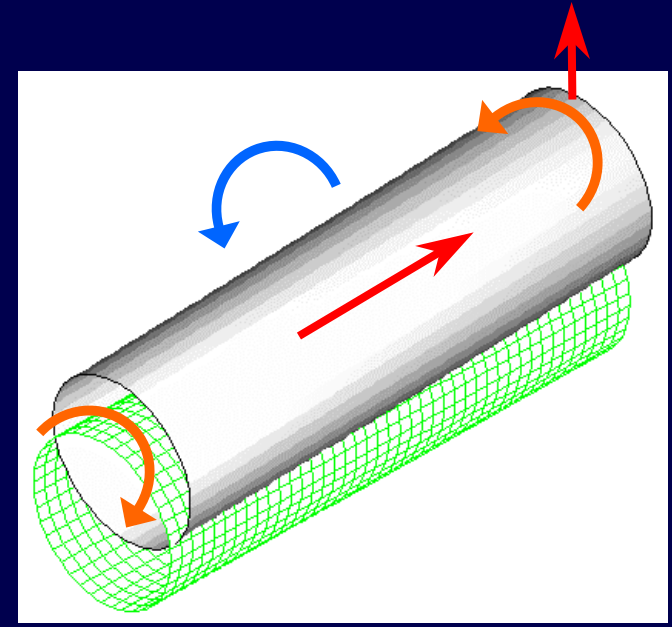
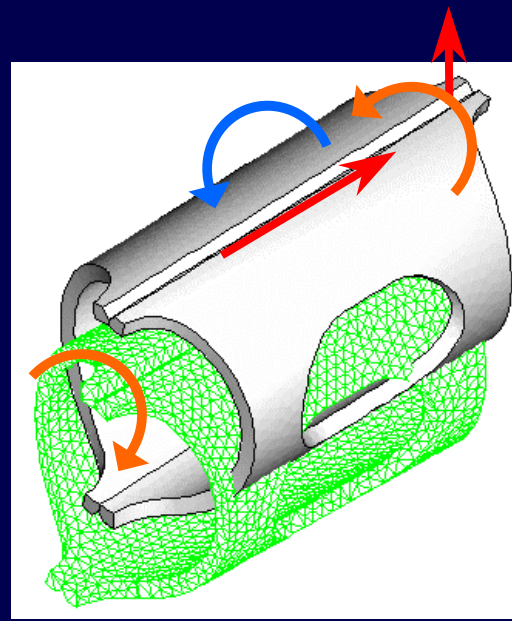
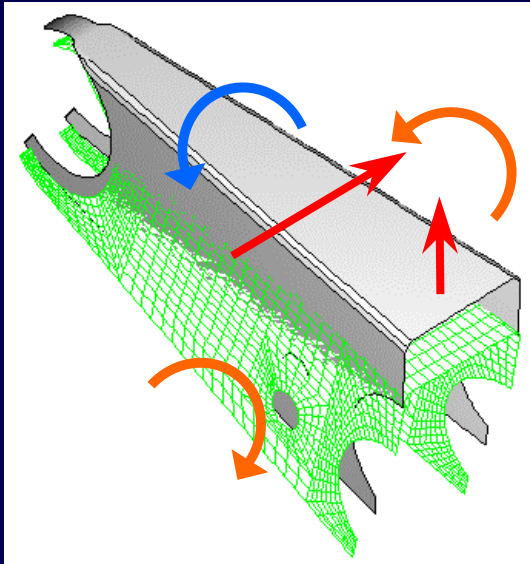


# Stress Analysis - Interpretation



*Adding value through knowledge*

## ■ Displacement Direction

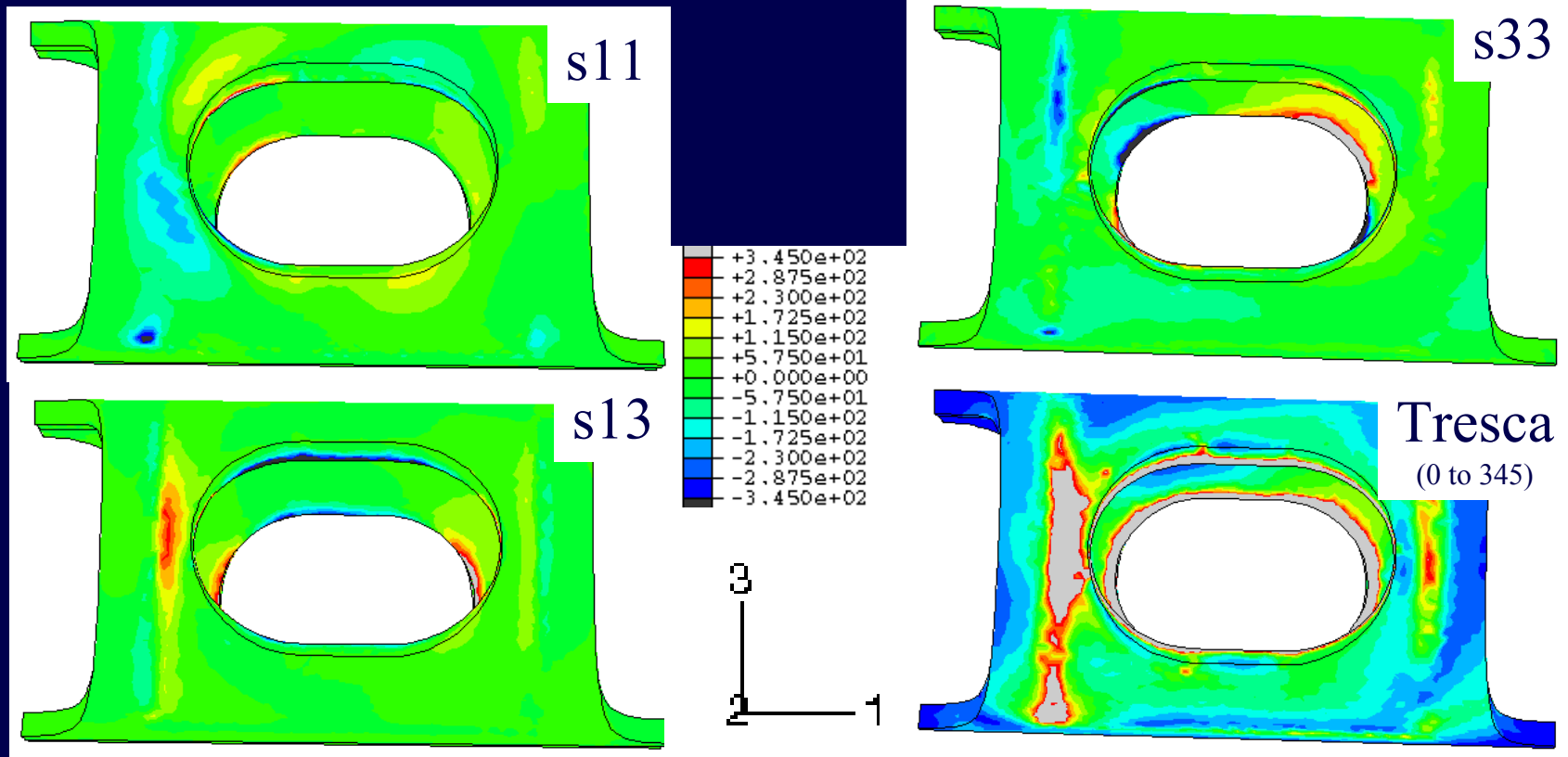


# Stress Analysis - Results



Adding value through knowledge

## ■ Tramp Manoeuvre - Stress Contours in Wrap Plate (Front)

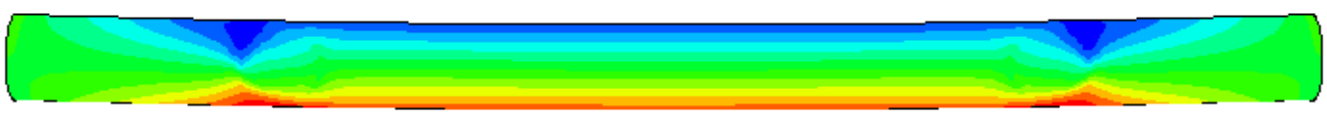
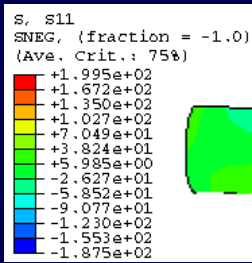


# Stress Analysis - Interpretation

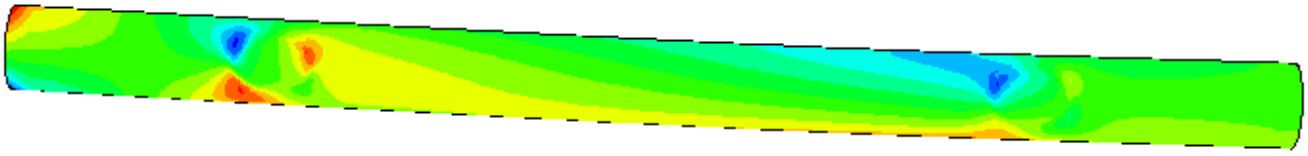
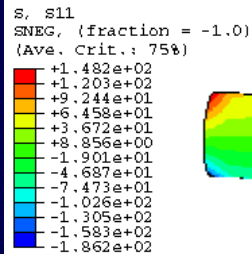


Adding value through knowledge

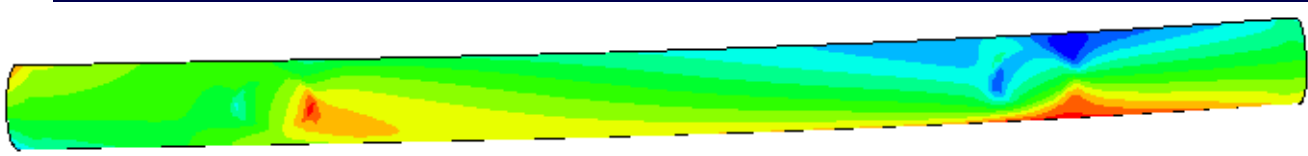
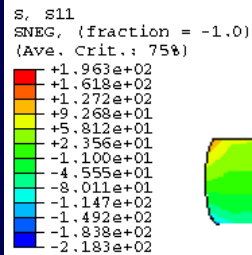
## ■ S11 Stress in Axle Front for all Loadcase



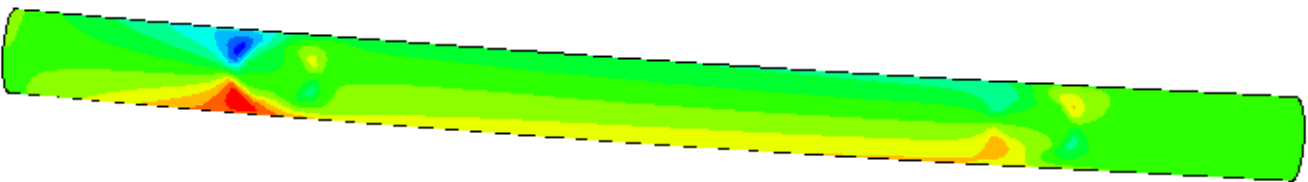
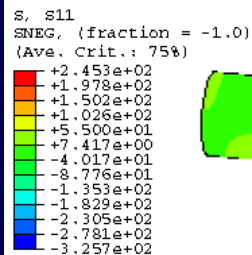
1.75g  
Bump



Roll



Scrub



Tramp

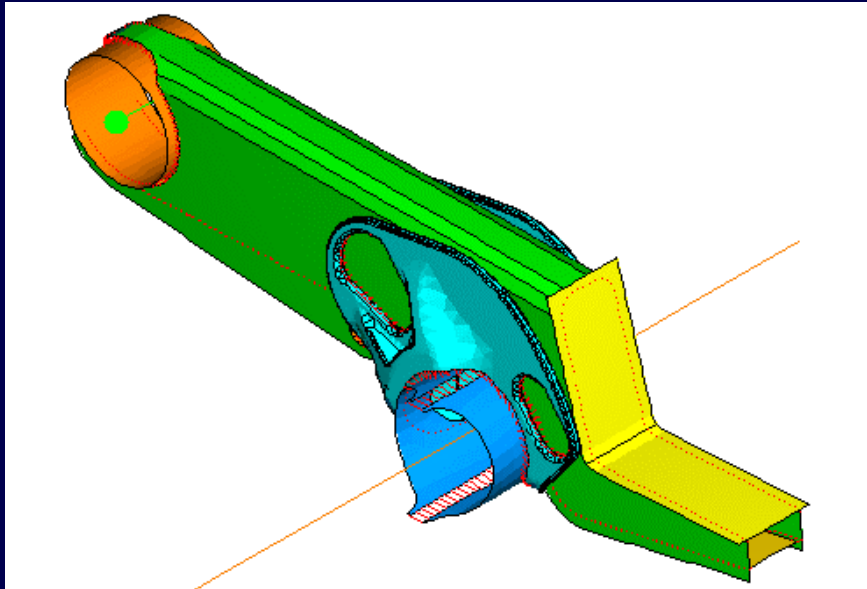


# Design Improvement



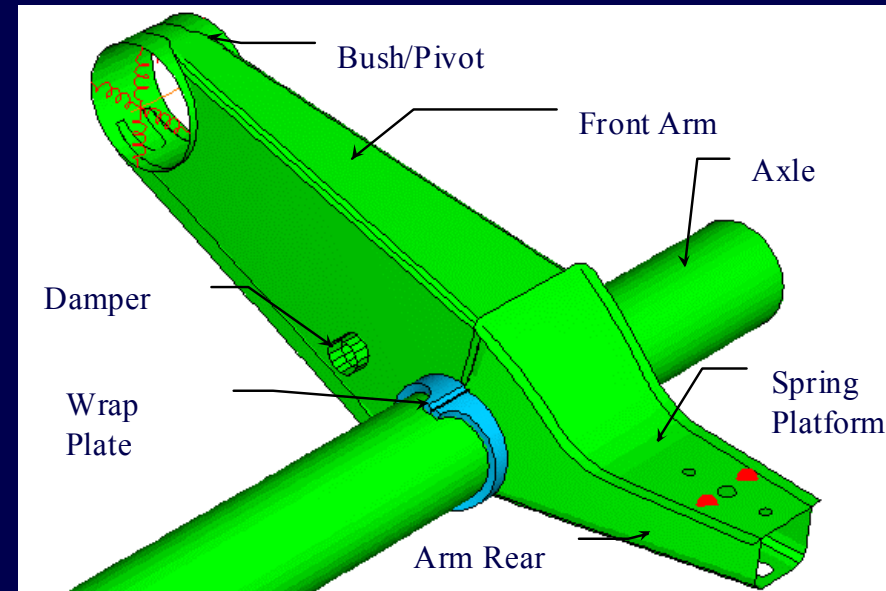
*Adding value through knowledge*

- **Improve the cutout radii**
- **Change the angular orientation of the Side Plate**



Original design

Fatigue life < 20,000 cycles



Improved design

Fatigue life > 35,000 cycles

The End